

CHAPTER 10

## EELE 3332 – Electromagnetic II Chapter 10

### Electromagnetic Wave Propagation

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### 10.7 Power and the Poynting Vector

- \* Energy can be transported from one point (where a transmitter is located) to another point (with a receiver) by means of EM waves.
- \* The rate of energy transportation can be obtained from Maxwell's equations:

Using Maxwell equation:  $\nabla \times \mathbf{H} = \sigma \mathbf{E} + \epsilon \frac{\partial \mathbf{E}}{\partial t}$

Dotting both sides with  $\mathbf{E}$ :

$$\mathbf{E} \cdot (\nabla \times \mathbf{H}) = \sigma E^2 + \epsilon \frac{\partial E^2}{\partial t}$$

But from vector identities:  $\nabla \cdot (\mathbf{H} \times \mathbf{E}) = \mathbf{E} \cdot (\nabla \times \mathbf{H}) - \mathbf{H} \cdot (\nabla \times \mathbf{E})$

$$\mathbf{E} \cdot (\nabla \times \mathbf{H}) = \mathbf{H} \cdot (\nabla \times \mathbf{E}) + \nabla \cdot (\mathbf{H} \times \mathbf{E})$$

$$\rightarrow \mathbf{H} \cdot (\nabla \times \mathbf{E}) + \nabla \cdot (\mathbf{H} \times \mathbf{E}) = \sigma E^2 + \epsilon \frac{\partial E^2}{\partial t} \quad \dots (1)$$

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Using Maxwell equation :  $\nabla \times \mathbf{E} = -\mu \frac{\partial \mathbf{H}}{\partial t}$ , Dotting both sides with  $\mathbf{H}$ :

$$\mathbf{H} \cdot (\nabla \times \mathbf{E}) = \mathbf{H} \cdot \left( -\mu \frac{\partial \mathbf{H}}{\partial t} \right) = -\frac{\mu}{2} \frac{\partial H^2}{\partial t}$$

Substitute in equation (1):  $\mathbf{H} \cdot (\nabla \times \mathbf{E}) + \nabla \cdot (\mathbf{H} \times \mathbf{E}) = \sigma E^2 + \epsilon \frac{\partial E^2}{\partial t}$

$$-\frac{\mu}{2} \frac{\partial H^2}{\partial t} - \nabla \cdot (\mathbf{E} \times \mathbf{H}) = \sigma E^2 + \epsilon \frac{\partial E^2}{\partial t}$$

$$\rightarrow \nabla \cdot (\mathbf{E} \times \mathbf{H}) = -\sigma E^2 - \frac{1}{2} \epsilon \frac{\partial E^2}{\partial t} - \frac{\mu}{2} \frac{\partial H^2}{\partial t}$$

Take volume integral of both sides:

$$\int_V \nabla \cdot (\mathbf{E} \times \mathbf{H}) dv = -\frac{\partial}{\partial t} \int_V \left[ \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right] dv - \int_V \sigma E^2 dv$$

Applying the divergence theorem to the left hand side:

$$\oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} = -\frac{\partial}{\partial t} \int_V \left[ \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right] dv - \int_V \sigma E^2 dv$$

### Power and the Poynting Vector

Poynting's theorem

$$\oint_S (\mathbf{E} \times \mathbf{H}) \cdot d\mathbf{S} = -\frac{\partial}{\partial t} \int_V \left[ \frac{1}{2} \epsilon E^2 + \frac{1}{2} \mu H^2 \right] dv - \int_V \sigma E^2 dv$$

Total power leaving the volume

Rate of decrease in energy stored in electric and magnetic fields

Ohmic power dissipated

the *Poynting Vector* (Watts/m<sup>2</sup>) is defined as:

$$\mathbf{\rho} = \mathbf{E} \times \mathbf{H}$$

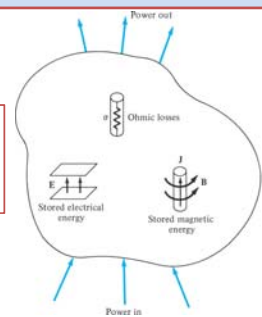
It represents the instantaneous power density vector associated with the EM field at a given point.

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### Power and the Poynting Vector

**Poynting theorem:** states that the net power flowing out of a given volume  $\nu$  is equal to the time rate of decrease in the energy stored with  $\nu$  minus the ohmic losses.

Illustration of power balance for EM fields.



Note that  $\phi = \mathbf{E} \times \mathbf{H}$  is normal to both E and H and is therefore along the direction of propagation  $\mathbf{a}_k$

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### Power and the Poynting Vector

Assume that

$$E(z, t) = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \mathbf{a}_x$$

then  $H(z, t) = \frac{E_0}{|\eta|} e^{-\alpha z} \cos(\omega t - \beta z - \theta_\eta) \mathbf{a}_y$

and  $\phi(z, t) = \mathbf{E} \times \mathbf{H} = \frac{E_0^2}{|\eta|} e^{-2\alpha z} \cos(\omega t - \beta z) \cos(\omega t - \beta z - \theta_\eta) \mathbf{a}_z$

$$\phi(z, t) = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} [\cos \theta_\eta + \cos(2\omega t - 2\beta z - \theta_\eta)] \mathbf{a}_z$$

since  $\cos A \cos B = \frac{1}{2} [\cos(A - B) + \cos(A + B)]$

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### Power and the Poynting Vector

The time-average Poynting vector  $\phi_{ave}(z)$  over the period  $T=2\pi/\omega$  is:

$$\phi_{ave}(z) = \frac{1}{T} \int_0^T \phi(z, t) dt$$

It can also be found by:

$$\phi_{ave}(z) = \frac{1}{2} \text{Re}(\mathbf{E}_s \times \mathbf{H}_s^*)$$

For  $\phi(z, t) = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} [\cos \theta_\eta + \cos(2\omega t - 2\beta z - \theta_\eta)] \mathbf{a}_z$

$$\rightarrow \phi_{ave}(z) = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} \cos \theta_\eta \mathbf{a}_z$$

The total time-average power crossing a given surface S is given by:

$$P_{ave} = \int_S \phi_{ave} \cdot d\mathbf{S}$$

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### Power and the Poynting Vector

$\phi(x, y, z, t) \rightarrow$  Poynting vector (time-varying vector)  $\rightarrow$  (watts/m<sup>2</sup>)

$$\phi(x, y, z, t) = \mathbf{E} \times \mathbf{H}$$

$\phi_{ave}(x, y, z) \rightarrow$  time-average of Poynting vector (time-invariant vector)  $\rightarrow$  (watts/m<sup>2</sup>)

$$\phi_{ave} = \frac{1}{T} \int_0^T \phi(x, y, z, t) dt$$

$$\phi_{ave} = \frac{1}{2} \text{Re}(\mathbf{E}_s \times \mathbf{H}_s^*)$$

$$\phi_{ave}(z) = \frac{E_0^2}{2|\eta|} e^{-2\alpha z} \cos \theta_\eta \mathbf{a}_z \quad (\text{for } \mathbf{E} = E_0 e^{-\alpha z} \cos(\omega t - \beta z) \mathbf{a}_x)$$

$P_{ave} \rightarrow$  total time-average power through a surface (scalar)  $\rightarrow$  watts

$$P_{ave} = \int_S \phi_{ave} \cdot d\mathbf{S}$$

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### Example 10.7

In a nonmagnetic medium

$$E = 4 \sin(2\pi \times 10^7 t - 0.8x) \mathbf{a}_z \text{ V/m}$$

Find

- $\epsilon_r$ ,  $\eta$
- The time-average power carried by the wave
- The total power crossing  $100 \text{ cm}^2$  of plane  $2x + y = 5$

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### Example 10.7 - Solution

(a) Since  $\alpha=0$  and  $\beta \neq \omega/c$ , the medium is not free space but a lossless medium.

$$\beta = 0.8, \quad \omega = 2\pi \times 10^7, \quad \mu = \mu_0 \text{ (nonmagnetic)}, \quad \epsilon = \epsilon_0 \epsilon_r$$

Hence

$$\beta = \omega \sqrt{\mu \epsilon} = \omega \sqrt{\mu_0 \epsilon_0 \epsilon_r} = \frac{\omega}{c} \sqrt{\epsilon_r}$$

or

$$\sqrt{\epsilon_r} = \frac{\beta c}{\omega} = \frac{0.8(3 \times 10^8)}{2\pi \times 10^7} = \frac{12}{\pi}$$

$$\epsilon_r = 14.59$$

$$\eta = \sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_0}{\epsilon_0 \epsilon_r}} = \frac{120\pi}{\sqrt{\epsilon_r}} = 120\pi \cdot \frac{\pi}{12} = 10\pi^2 = 98.7 \Omega$$

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### Example 10.7 - Solution

$$(b) \quad \phi = \mathbf{E} \times \mathbf{H} = \frac{E_o^2}{\eta} \sin^2(\omega t - \beta x) \mathbf{a}_x$$

$$\phi_{ave} = \frac{1}{T} \int_0^T \phi dt = \frac{E_o^2}{2\eta} \mathbf{a}_x = \frac{16}{2 \times 10\pi^2} \mathbf{a}_x = 81 \mathbf{a}_x \text{ mW/m}^2$$

(c) On plane  $2x + y = 5$  (see Example 3.5 or 8.5),

$$\mathbf{a}_n = \frac{2\mathbf{a}_x + \mathbf{a}_y}{\sqrt{5}}$$

Hence the total power is

$$P_{ave} = \int \phi_{ave} dS = \phi_{ave} \cdot S \mathbf{a}_n = (81 \times 10^{-3} \mathbf{a}_x) \cdot (100 \times 10^{-4}) \left[ \frac{2\mathbf{a}_x + \mathbf{a}_y}{\sqrt{5}} \right]$$

$$= \frac{162 \times 10^{-5}}{\sqrt{5}} = 724.5 \mu\text{W}$$

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### 10.8 Reflection of a plane wave at normal incidence

□ When a plane wave from one medium meets a different medium, it is partly **reflected** and partly **transmitted**.

□ The proportion of the incident wave that is reflected or transmitted depends on the parameters ( $\epsilon, \mu, \sigma$ ) of the two media involved.

□ **Normal** incidence (plane wave is normal to the boundary) and **oblique** incidence will be studied.

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### Reflection of a plane wave at normal incidence

Suppose a plane wave propagating along the +z direction is incident normally on the boundary z=0 between medium 1 (z<0) characterised by  $\epsilon_1, \mu_1, \sigma_1$  and medium 2 (z>0) characterised by  $\epsilon_2, \mu_2, \sigma_2$ .

The diagram shows a coordinate system with x, y, and z axes. The boundary is at z=0. In Medium 1 (z < 0), an incident wave with electric field  $E_i$  (pointing up) and magnetic field  $H_i$  (pointing right) propagates in the +z direction. A reflected wave with electric field  $E_r$  (pointing up) and magnetic field  $H_r$  (pointing left) propagates in the -z direction. In Medium 2 (z > 0), a transmitted wave with electric field  $E_t$  (pointing up) and magnetic field  $H_t$  (pointing right) propagates in the +z direction. A hand gesture on the right illustrates the right-hand rule: the index finger points in the direction of the electric field (E), the middle finger points in the direction of the magnetic field (H), and the thumb points in the direction of the wave propagation (K).

### Reflection of a plane wave at normal incidence

**Incident Wave**  
 $(E_i, H_i)$  is traveling along  $+a_z$  in medium 1.  
 Assume the electric and magnetic field (in phasor form) as follows:

$$E_{is}(z) = E_{i0} e^{-\gamma_1 z} a_x, \text{ then}$$

$$H_{is}(z) = H_{i0} e^{-\gamma_1 z} a_y = \frac{E_{i0}}{\eta_1} e^{-\gamma_1 z} a_y$$

$E_{i0}$  is magnitude of the incident electric field at z=0

The diagram shows a coordinate system with x, y, and z axes. The boundary is at z=0. In Medium 1 (z < 0), an incident wave with electric field  $E_i$  (pointing up) and magnetic field  $H_i$  (pointing right) propagates in the +z direction. A reflected wave with electric field  $E_r$  (pointing up) and magnetic field  $H_r$  (pointing left) propagates in the -z direction. In Medium 2 (z > 0), a transmitted wave with electric field  $E_t$  (pointing up) and magnetic field  $H_t$  (pointing right) propagates in the +z direction.

### Reflection of a plane wave at normal incidence

**Reflected Wave**  
 $(E_r, H_r)$  is traveling along  $-a_z$  in medium 1.

$$\text{If } E_{rs}(z) = E_{r0} e^{\gamma_1 z} a_x, \text{ then}$$

$$H_{rs}(z) = H_{r0} e^{\gamma_1 z} (-a_y) = -\frac{E_{r0}}{\eta_1} e^{\gamma_1 z} a_y$$

$E_{r0}$  is magnitude of the reflected electric field at z=0

The diagram shows a coordinate system with x, y, and z axes. The boundary is at z=0. In Medium 1 (z < 0), an incident wave with electric field  $E_i$  (pointing up) and magnetic field  $H_i$  (pointing right) propagates in the +z direction. A reflected wave with electric field  $E_r$  (pointing up) and magnetic field  $H_r$  (pointing left) propagates in the -z direction. In Medium 2 (z > 0), a transmitted wave with electric field  $E_t$  (pointing up) and magnetic field  $H_t$  (pointing right) propagates in the +z direction.

### Reflection of a plane wave at normal incidence

**Transmitted Wave**  
 $(E_t, H_t)$  is traveling along  $+a_z$  in medium 2.

$$\text{If } E_{ts}(z) = E_{t0} e^{-\gamma_2 z} a_x, \text{ then}$$

$$H_{ts}(z) = H_{t0} e^{-\gamma_2 z} a_y = \frac{E_{t0}}{\eta_2} e^{-\gamma_2 z} a_y$$

$E_{t0}$  is magnitude of the transmitted electric field at z=0

The diagram shows a coordinate system with x, y, and z axes. The boundary is at z=0. In Medium 1 (z < 0), an incident wave with electric field  $E_i$  (pointing up) and magnetic field  $H_i$  (pointing right) propagates in the +z direction. A reflected wave with electric field  $E_r$  (pointing up) and magnetic field  $H_r$  (pointing left) propagates in the -z direction. In Medium 2 (z > 0), a transmitted wave with electric field  $E_t$  (pointing up) and magnetic field  $H_t$  (pointing right) propagates in the +z direction.

### Reflection of a plane wave at normal incidence

Field in medium 1:  $E_1 = E_i + E_r$ ,  $H_1 = H_i + H_r$   
 Field in medium 2:  $E_2 = E_t$ ,  $H_2 = H_t$

→ Since the waves are transverse, E and H fields are entirely tangential to the interface.  
 → Applying the boundary conditions at the interface  $z = 0$ :  
 ( $E_{1t} = E_{2t}$  and  $H_{1t} = H_{2t}$ )  
 then :

$$E_i(0) + E_{r0}(0) = E_{t0}(0) \rightarrow E_{i0} + E_{r0} = E_{t0}$$

$$H_i(0) + H_r(0) = H_t(0) \rightarrow \frac{1}{\eta_1}(E_{i0} - E_{r0}) = \frac{E_{t0}}{\eta_2}$$

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### Reflection of a plane wave at normal incidence

From the last two equations:

$$E_{r0} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} E_{i0}$$

→ Reflection Coefficient  $\Gamma = \frac{E_{r0}}{E_{i0}} = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$ , or  $E_{r0} = \Gamma E_{i0}$

and  $E_{t0} = \frac{2\eta_2}{\eta_2 + \eta_1} E_{i0}$

→ Transmission Coefficient  $\tau = \frac{E_{t0}}{E_{i0}} = \frac{2\eta_2}{\eta_2 + \eta_1}$ , or  $E_{t0} = \tau E_{i0}$

Note that:

- $1 + \Gamma = \tau$
- Both  $\Gamma$  and  $\tau$  are dimensionless and may be complex.  
( $\Gamma$  and  $\tau$  are real for lossless media, and complex for lossy media)
- $0 \leq |\Gamma| \leq 1$

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### Reflection of a plane wave at normal incidence

**When medium 1 is a perfect dielectric (lossless,  $\sigma_1=0$ ), and medium 2 is a perfect conductor ( $\sigma_2=\infty$ ):**

For conductor $\eta = \sqrt{\frac{\omega\mu}{\sigma}} \angle 45^\circ$	Medium 1 <b>a perfect dielectric</b> (lossless, $\sigma_1=0$ )	Medium 2 <b>a perfect conductor</b> ( $\sigma_2=\infty$ )
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➤  $\eta_2 = 0 \rightarrow \Gamma = -1 \rightarrow \tau = 0$

➤ The wave is totally reflected and there is no transmitted wave ( $E_2 = 0$ ).

➤ The totally reflected wave combines with the incident wave to form a **standing wave**.

➤ A **standing wave** "stands" and does not travel; it consists of two travelling waves ( $E_i$  and  $E_r$ ) of equal amplitudes but in opposite directions.

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### Reflection of a plane wave at normal incidence

The standing wave in medium 1 is:

$E_{1s} = E_{is} + E_{rs} = (E_{i0}e^{-\gamma_1 z} + E_{r0}e^{\gamma_1 z}) a_x$	Medium 1 <b>a perfect dielectric</b> (lossless, $\sigma_1=0$ )	Medium 2 <b>a perfect conductor</b> ( $\sigma_2=\infty$ )
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But  $\Gamma = \frac{E_{r0}}{E_{i0}} = -1$ ,  $\sigma_1 = 0$ ,  $\alpha_1 = 0$ ,  $\gamma_1 = j\beta_1$

$$E_{1s} = -E_{i0} (e^{j\beta_1 z} - e^{-j\beta_1 z}) a_x$$

or  $E_{1s} = -2jE_{i0} \sin \beta_1 z a_x$  (since  $\sin A = \frac{e^{jA} - e^{-jA}}{2j}$ )

Thus  $E_{1s} = \text{Re}(E_{1s} e^{j\omega t})$ , or  $E_{1s} = 2E_{i0} \sin \beta_1 z \sin \omega t a_x$

Similarly, it can be shown that:  $H_{1s} = \frac{2E_{i0}}{\eta_1} \cos \beta_1 z \cos \omega t a_y$

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### Reflection of a plane wave at normal incidence

$\sigma_1 = 0$        $\sigma_2 = \infty$

**Standing waves**  $E = 2E_{0i} \sin \beta_1 z \sin \omega t \mathbf{a}_x$ . The curves 0, 1, 2, 3, 4, ..., are, respectively, at times  $t = 0, T/8, T/4, 3T/8, T/2, \dots$ ;  $\lambda = 2\pi/\beta_1$ .

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### Standing Waves Examples

<http://www.walter-fendt.de/ph14e/stwaverefl.htm>

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### Reflection of a plane wave at normal incidence

**Medium 1 : perfect dielectric  $\sigma_1=0$**   
**Medium 2: perfect dielectric  $\sigma_2=0$**

- $\eta_1$  and  $\eta_2$  are real and so are  $\Gamma$  and  $\tau$ .
- There is a standing wave in medium 1 but there is also a transmitted wave in medium 2. (*incident wave is partly reflected and partly transmitted*).
- However, the incident and reflected waves have amplitudes that are not equal in magnitude.
- Two cases:
  - case 1: when  $\eta_2 > \eta_1$
  - case 2: when  $\eta_2 < \eta_1$

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### CASE 1

**Medium 1 : perfect dielectric  $\sigma_1=0$ , Medium 2: perfect dielectric  $\sigma_2=0$**

If  $\eta_2 > \eta_1$ ,  $\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$ ,  $\Gamma > 0$ ,  $E_{1s} = E_{is} + E_{rs} = E_{oi} (e^{-j\beta_1 z} + \Gamma e^{+j\beta_1 z})$   
 $= E_{oi} e^{-j\beta_1 z} (1 + |\Gamma| e^{+2j\beta_1 z})$   
 $\rightarrow |E_{1s}| = E_{oi} |1 + |\Gamma| e^{+2j\beta_1 z}|$

$\Gamma = |\Gamma| e^{j\theta} = |\Gamma| \angle \theta^\circ$   
 $\tau$  and  $\Gamma$  are real

$|E_1|$  is maximum when  $e^{+2j\beta_1 z} = 1 \rightarrow |E_1|_{\max} = E_{oi} (1 + |\Gamma|)$   
 $-2\beta_1 z_{\max} = 0, 2\pi, 4\pi, 6\pi \dots \rightarrow z_{\max} = -\frac{n\pi}{\beta_1} = -\frac{n\lambda_1}{2} \quad n = 0, 1, 2, 3$   
 or  $-\beta_1 z_{\max} = 0, \pi, 2\pi, 3\pi, \dots$

$|E_1|$  is minimum when  $e^{+2j\beta_1 z} = -1 \rightarrow |E_1|_{\min} = E_{oi} (1 - |\Gamma|)$   
 $-2\beta_1 z_{\min} = \pi, 3\pi, 5\pi \dots$  or  $-\beta_1 z_{\min} = \frac{\pi}{2}, \frac{3\pi}{2}, \frac{5\pi}{2} \dots$   
 $z_{\min} = -\frac{(2n+1)\pi}{2\beta_1} = -\frac{(2n+1)\lambda_1}{4} \quad n = 0, 1, 2, 3$

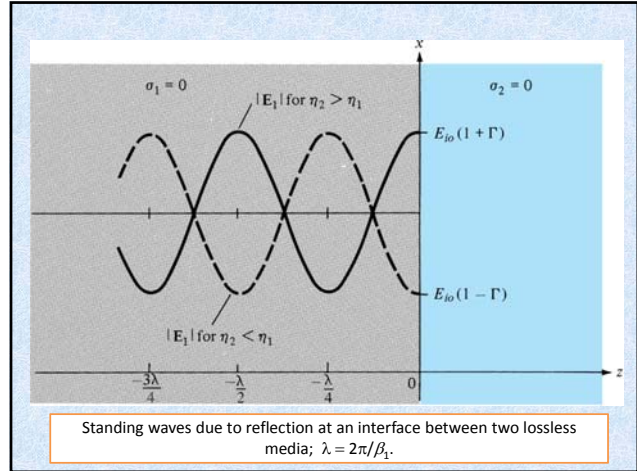
**CASE 2**

**Medium 1 : perfect dielectric  $\sigma_1=0$ , Medium 2: perfect dielectric  $\sigma_2=0$**

If  $\eta_2 < \eta_1$ ,  $\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$ ,  $\Gamma < 0$ ,  $E_{1s} = E_{is} + E_{rs} = E_{oi} (e^{-j\beta_1 z} + \Gamma e^{+j\beta_1 z})$   
 $= E_{oi} e^{-j\beta_1 z} (1 - |\Gamma| e^{+2j\beta_1 z})$   
 $\Gamma = |\Gamma| e^{j\tau} = |\Gamma| \angle 180^\circ$   
 $\tau$  and  $\Gamma$  are real  
 $\rightarrow |E_{1s}| = E_{oi} |1 - |\Gamma| e^{+2j\beta_1 z}|$

$|E_1|$  is maximum when  $e^{+2j\beta_1 z} = -1 \rightarrow |E_1|_{\max} = E_{oi} (1 + |\Gamma|)$   
 $-2\beta_1 z_{\max} = \pi, 3\pi, 5\pi, \dots$  or  $-\beta_1 z_{\max} = \frac{\pi}{2}, \frac{3\pi}{2}, \frac{5\pi}{2}, \dots$   
 $z_{\max} = -\frac{(2n+1)\pi}{2\beta_1} = -\frac{(2n+1)\lambda_1}{4}$   $n = 0, 1, 2, 3$

$|E_1|$  is minimum when  $e^{+2j\beta_1 z} = 1 \rightarrow |E_1|_{\min} = E_{oi} (1 - |\Gamma|)$   
 $-2\beta_1 z_{\min} = 0, 2\pi, 4\pi, 6\pi, \dots$   $\rightarrow z_{\min} = -\frac{n\pi}{\beta_1} = -\frac{n\lambda_1}{2}$   $n = 0, 1, 2, 3$   
 or  $-\beta_1 z_{\min} = 0, \pi, 2\pi, 3\pi, \dots$



**Standing Wave Ratio, SWR**

- Measures the amount of reflections, the more reflections, the larger the standing wave that is formed.
- The ratio of  $|E_1|_{\max}$  to  $|E_1|_{\min}$

$$s = \frac{|E_1|_{\max}}{|E_1|_{\min}} = \frac{|H_1|_{\max}}{|H_1|_{\min}} = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

or  $|\Gamma| = \frac{s - 1}{s + 1}$

➤ Since  $0 \leq |\Gamma| \leq 1$ , it follows that  $1 \leq s \leq \infty$ .

- When  $\Gamma=0$ ,  $s=1$ , no reflection, total transmission.
- When  $|\Gamma|=1$ ,  $s=\infty$ , no transmission, total reflection.

➤  $s$  is dimensionless, expressed in decibels (dB) as:  $s_{dB} = 20 \log_{10} s$

**Example 10.8**

In freespace ( $z \leq 0$ ), a plane wave with  $\mathbf{H}_i = 10 \cos(10^8 t - \beta z) \mathbf{a}_x$  mA/m is incident normally on a lossless medium ( $\epsilon = 2\epsilon_0, \mu = 8\mu_0$ ) in region  $z \geq 0$ . Determine the reflected wave  $\mathbf{H}_r$ ,  $\mathbf{E}_r$  and the transmitted wave  $\mathbf{H}_t$ ,  $\mathbf{E}_t$

**Solution :**

$$\beta_1 = \frac{\omega}{c} = \frac{10^8}{3 \times 10^8} = \frac{1}{3}$$

$$\eta_1 = \eta_0 = 120\pi$$

$$\beta_2 = \omega \sqrt{\mu \epsilon} = \omega \sqrt{\mu_0 \epsilon_0} \sqrt{\mu_r \epsilon_r}$$

$$\beta_2 = \frac{\omega}{c} (4) = 4\beta_1 = \frac{4}{3}$$

$$\eta_2 = \sqrt{\frac{\mu}{\epsilon}} = \sqrt{\frac{\mu_0}{\epsilon_0}} \sqrt{\frac{\mu_r}{\epsilon_r}} = 2\eta_0$$

**Example 10.8 – solution continued**

Given that  $\mathbf{H}_i = 10 \cos(10^8 t - \beta_1 z) \mathbf{a}_x$  we expect that

$$\mathbf{E}_i = E_{io} \cos(10^8 t - \beta_1 z) \mathbf{a}_{Ei}$$

where  $\mathbf{a}_{Ei} = \mathbf{a}_{Hi} \times \mathbf{a}_{ki} = \mathbf{a}_x \times \mathbf{a}_z = -\mathbf{a}_y$  and  $E_{io} = \eta_1 H_{io} = 10 \eta_o$

Hence,  $\mathbf{E}_i = -10 \eta_o \cos(10^8 t - \beta_1 z) \mathbf{a}_y$  mV/m

$$\text{Now } \frac{E_{ro}}{E_{io}} = \Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1} = \frac{2\eta_o - \eta_o}{2\eta_o + \eta_o} = \frac{1}{3}, \quad E_{ro} = \frac{1}{3} E_{io}$$

$$\text{Thus } \mathbf{E}_r = -\frac{10}{3} \eta_o \cos\left(10^8 t + \frac{1}{3} z\right) \mathbf{a}_y \text{ mV/m}$$

from which we easily obtain  $\mathbf{H}_r$  as

$$\mathbf{H}_r = -\frac{10}{3} \cos\left(10^8 t + \frac{1}{3} z\right) \mathbf{a}_x \text{ mA/m}$$

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**Example 10.8 – solution continued**

Similarly,

$$\frac{E_{to}}{E_{io}} = \tau = 1 + \Gamma = \frac{4}{3} \text{ or } E_{to} = \frac{4}{3} E_{io}$$

Thus

$$\mathbf{E}_t = E_{to} \cos\left(10^8 t + \beta_2 z\right) \mathbf{a}_{Et}$$

where  $\mathbf{a}_{Et} = \mathbf{a}_{Et} = -\mathbf{a}_y$ . Hence,

$$\mathbf{E}_t = -\frac{40}{3} \eta_o \cos\left(10^8 t - \frac{4}{3} z\right) \mathbf{a}_y \text{ mV/m}$$

from which we obtain

$$\mathbf{H}_t = \frac{20}{3} \cos\left(10^8 t - \frac{4}{3} z\right) \mathbf{a}_x \text{ mA/m}$$

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**Example 10.9**

Given a uniform plane wave in air as

$$\mathbf{E}_i = 40 \cos(\omega t - \beta z) \mathbf{a}_x + 30 \sin(\omega t - \beta z) \mathbf{a}_y \text{ V/m}$$

- Find  $\mathbf{H}_i$ .
- If the wave encounters a perfectly conducting plate normal to the  $z$  axis at  $z = 0$ , find the reflected wave  $\mathbf{E}_r$  and  $\mathbf{H}_r$ .
- What are the total  $\mathbf{E}$  and  $\mathbf{H}$  fields for  $z \leq 0$  ?
- Calculate the time-average Poynting vectors for  $z \leq 0$  and  $z \geq 0$ .

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**Example 10.9 -solution****Solution**

(a) This is similar to the problem in Example 10.3.

We may treat the wave as consisting of two waves  $\mathbf{E}_{i1}$  and  $\mathbf{E}_{i2}$  where

$$\mathbf{E}_{i1} = 40 \cos(\omega t - \beta z) \mathbf{a}_x, \quad \mathbf{E}_{i2} = 30 \sin(\omega t - \beta z) \mathbf{a}_y$$

At atmospheric pressure, air has  $\epsilon_r = 1.0006 \cong 1$ .

Thus air may be regarded as free space.

Let  $\mathbf{H}_i = \mathbf{H}_{i1} + \mathbf{H}_{i2}$

$$\mathbf{H}_{i1} = H_{i1o} \cos(\omega t - \beta z) \mathbf{a}_{H1}$$

$$H_{i1o} = \frac{E_{i1o}}{\eta_o} = \frac{40}{120\pi} = \frac{1}{3\pi}$$

$$\mathbf{a}_{H1} = \mathbf{a}_k \times \mathbf{a}_{E1} = \mathbf{a}_z \times \mathbf{a}_x = \mathbf{a}_y$$

Hence  $\mathbf{H}_{i1} = \frac{1}{3\pi} \cos(\omega t - \beta z) \mathbf{a}_y$

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**Example 10.9 -solution**

Similarly,

$$\mathbf{H}_{i2} = H_{i2o} \sin(\omega t - \beta z) \mathbf{a}_{H_2}$$

where

$$H_{i2o} = \frac{E_{i2o}}{\eta_o} = \frac{30}{120\pi} = \frac{1}{4\pi}$$

$$\mathbf{a}_{H_2} = \mathbf{a}_k \times \mathbf{a}_E = \mathbf{a}_z \times \mathbf{a}_y = -\mathbf{a}_x$$

Hence

$$\mathbf{H}_{i2} = -\frac{1}{4\pi} \sin(\omega t - \beta z) \mathbf{a}_x$$

and

$$\mathbf{H}_i = \mathbf{H}_{i1} + \mathbf{H}_{i2} = -\frac{1}{4\pi} \sin(\omega t - \beta z) \mathbf{a}_x + \frac{1}{3\pi} \cos(\omega t - \beta z) \mathbf{a}_y \text{ mA/m}$$

This problem can also be solved using Method 2 of Example 10.3.

**Example 10.9 -solution**

(b) Since medium 2 is perfectly conducting,

$$\frac{\sigma_2}{\omega \epsilon_2} \gg 1 \rightarrow \eta_2 \ll \eta_1$$

that is  $\Gamma \approx -1$ ,  $\tau = 0$

showing that the incident  $\mathbf{E}$  and  $\mathbf{H}$  fields are totally reflected.

$$E_{ro} = \Gamma E_{io} = -E_{io}$$

Hence,  $\mathbf{E}_r = -40 \cos(\omega t + \beta z) \mathbf{a}_x - 30 \sin(\omega t + \beta z) \mathbf{a}_y \text{ V/m}$

$$\mathbf{H}_r = \frac{1}{3\pi} \cos(\omega t + \beta z) \mathbf{a}_y - \frac{1}{4\pi} \sin(\omega t + \beta z) \mathbf{a}_x \text{ A/m}$$

(c) The total fields in air

$$\mathbf{E}_i = \mathbf{E}_i + \mathbf{E}_r \text{ and } \mathbf{H}_i = \mathbf{H}_i + \mathbf{H}_r$$

can be shown to be standing wave.

The total fields in the conductor are  $\mathbf{E}_2 = \mathbf{E}_t = 0$ ,  $\mathbf{H}_2 = \mathbf{H}_t = 0$ .

**Example 10.9 -solution**

(d) For  $z \leq 0$ ,

$$\begin{aligned} \mathcal{P}_{1ave} &= \frac{|E_{1s}|^2}{2\eta_1} \mathbf{a}_k = \frac{1}{2\eta_o} [E_{io}^2 \mathbf{a}_z - E_{ro}^2 \mathbf{a}_z] \\ &= \frac{1}{240\pi} [(40^2 + 30^2) \mathbf{a}_z - (40^2 + 30^2) \mathbf{a}_z] = 0 \end{aligned}$$

For  $z \geq 0$ ,

$$\mathcal{P}_{2ave} = \frac{|E_{2s}|^2}{2\eta_2} \mathbf{a}_k = \frac{E_{to}^2}{2\eta_2} \mathbf{a}_z = 0$$

because the whole incident power is reflected.

**Oblique incidence**

- Wave arrives at an angle.
- Assume lossless media.
- Uniform plane wave in general form



$$E(\mathbf{r}, t) = E_o \cos(\mathbf{k} \cdot \mathbf{r} - \omega t) = \text{Re}[E_o e^{j(\mathbf{k} \cdot \mathbf{r} - \omega t)}]$$

$$\mathbf{r} = x\hat{a}_x + y\hat{a}_y + z\hat{a}_z \quad \text{position vector}$$

$$\mathbf{k} = k_x\hat{a}_x + k_y\hat{a}_y + k_z\hat{a}_z \quad \text{wave number or propagation vector}$$

$$k^2 = k_x^2 + k_y^2 + k_z^2 = \omega^2 \mu \epsilon$$

- For lossless unbounded media,  $k = \beta$

### Oblique incidence

$\triangleright \theta_i$  is *angle of incidence*.  
 $\triangleright$  The plane defined by propagation vector  $\mathbf{k}$  and a unit normal vector  $\mathbf{a}_n$  to the boundary is called *plane of incidence*.

### Oblique incidence

$$E_i = E_{io} \cos(k_{ix}x + k_{iy}y + k_{iz}z - \omega t)$$

$$E_r = E_{ro} \cos(k_{rx}x + k_{ry}y + k_{rz}z - \omega t)$$

$$E_t = E_{to} \cos(k_{tx}x + k_{ty}y + k_{tz}z - \omega t)$$

where  $k_i = k_r = \beta_1 = \omega\sqrt{\mu_1\epsilon_1}$   
 $k_t = \beta_2 = \omega\sqrt{\mu_2\epsilon_2}$

$$k_{ix} = \beta_1 \cos \theta_i$$

$$k_{iz} = \beta_1 \sin \theta_i$$

### Parallel Polarization

It's defined as  $\mathbf{E}$  is  $\parallel$  to incidence plane ( $\mathbf{E}$ -field lies in the  $xz$ -plane)

### Parallel Polarization

$$E_{is} = E_{io} (\cos \theta_i \mathbf{a}_x - \sin \theta_i \mathbf{a}_z) e^{-j\beta_1(x \sin \theta_i + z \cos \theta_i)}$$

$$H_{is} = \frac{E_{io}}{\eta_1} e^{-j\beta_1(x \sin \theta_i + z \cos \theta_i)} \mathbf{a}_y$$

$$E_{rs} = E_{ro} (\cos \theta_r \mathbf{a}_x + \sin \theta_r \mathbf{a}_z) e^{-j\beta_1(x \sin \theta_r - z \cos \theta_r)}$$

$$H_{rs} = -\frac{E_{ro}}{\eta_1} e^{-j\beta_1(x \sin \theta_r - z \cos \theta_r)} \mathbf{a}_y$$

### Parallel Polarization

$$E_{ts} = E_{to} (\cos \theta_t \mathbf{a}_x - \sin \theta_t \mathbf{a}_z) e^{-j\beta_2(x \sin \theta_t + z \cos \theta_t)}$$

$$H_{ts} = \frac{E_{to}}{\eta_2} e^{-j\beta_2(x \sin \theta_t + z \cos \theta_t)} \mathbf{a}_y$$

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### Parallel Polarization

Tangential components of E and H should be continuous at the boundary  $z=0$ ,

$$E_{io} (\cos \theta_i) e^{-j\beta_1 x \sin \theta_i} + E_{ro} (\cos \theta_r) e^{-j\beta_1 x \sin \theta_r} = E_{to} (\cos \theta_t) e^{-j\beta_2 x \sin \theta_t}$$

$$\frac{E_{io}}{\eta_1} e^{-j\beta_1 x \sin \theta_i} - \frac{E_{ro}}{\eta_1} e^{-j\beta_1 x \sin \theta_r} = \frac{E_{to}}{\eta_2} e^{-j\beta_2 x \sin \theta_t}$$

The exponential terms must be equal for the previous equations to be valid:  $\rightarrow \beta_1 \sin \theta_i = \beta_1 \sin \theta_r = \beta_2 \sin \theta_t$

or  $\theta_i = \theta_r$  (Incidence angle = reflection angle)

$$\rightarrow \frac{\beta_1}{\beta_2} = \frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}} = \frac{n_1}{n_2} \quad (\text{snell's law})$$

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### Parallel Polarization

Hence,

$$E_{io} \cos \theta_i + E_{ro} \cos \theta_r = E_{to} \cos \theta_t \quad (\text{x-components of E})$$

$$\frac{E_{io}}{\eta_1} - \frac{E_{ro}}{\eta_1} = \frac{E_{to}}{\eta_2} \quad (\text{y-component of H})$$

**Reflection coefficient**  $\Gamma_{\parallel} = \frac{E_{ro}}{E_{io}} = \frac{\eta_2 \cos \theta_t - \eta_1 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i}$ ,  $E_{ro} = \Gamma_{\parallel} E_{io}$

**Transmission coefficient**  $\tau_{\parallel} = \frac{E_{to}}{E_{io}} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_i}$ ,  $E_{to} = \tau_{\parallel} E_{io}$

where  $\tau_{\parallel} = (1 + \Gamma_{\parallel}) \frac{\cos \theta_i}{\cos \theta_t}$

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### Parallel Polarization - Brewster angle, $\theta_B$

- defined as the incidence angle at which the reflection coefficient is 0 (**all transmission**).

By setting  $\theta_i = \theta_B$  :-

$$\Gamma_{\parallel} = \frac{\eta_2 \cos \theta_t - \eta_1 \cos \theta_{B\parallel}}{\eta_2 \cos \theta_t + \eta_1 \cos \theta_{B\parallel}} = 0$$

$$\rightarrow \eta_2 \cos \theta_t = \eta_1 \cos \theta_{B\parallel}$$

or

$$\eta_2^2 (1 - \sin^2 \theta_t) = \eta_1^2 (1 - \sin^2 \theta_{B\parallel})$$

Since  $\frac{\sin \theta_t}{\sin \theta_i} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}}$ , and  $\theta_i = \theta_{B\parallel}$

$$\rightarrow \sin^2 \theta_{B\parallel} = \frac{1 - (\epsilon_1 \mu_2 / \epsilon_2 \mu_1)}{1 - (\epsilon_1 / \epsilon_2)^2}$$

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### Perpendicular Polarization

In this case, the E field is **perpendicular** to the plane of incidence (the xz-plane)

### Perpendicular Polarization

$$E_{is} = E_{io} e^{-j\beta_1(x\sin\theta_i + z\cos\theta_i)} \mathbf{a}_y$$

$$H_{is} = \frac{E_{io}}{\eta_1} (-\cos\theta_i \mathbf{a}_x + \sin\theta_i \mathbf{a}_z) e^{-j\beta_1(x\sin\theta_i + z\cos\theta_i)}$$

$$E_{rs} = E_{ro} e^{-j\beta_1(x\sin\theta_r - z\cos\theta_r)} \mathbf{a}_y$$

$$H_{rs} = \frac{E_{ro}}{\eta_1} (\cos\theta_r \mathbf{a}_x + \sin\theta_r \mathbf{a}_z) e^{-j\beta_1(x\sin\theta_r - z\cos\theta_r)}$$

### Perpendicular Polarization

$$E_{ts} = E_{to} e^{-j\beta_2(x\sin\theta_t + z\cos\theta_t)} \mathbf{a}_y$$

$$H_{ts} = \frac{E_{to}}{\eta_2} (-\cos\theta_t \mathbf{a}_x + \sin\theta_t \mathbf{a}_z) e^{-j\beta_2(x\sin\theta_t + z\cos\theta_t)}$$

### Perpendicular Polarization

*Tangential* components of E and H should be continuous at the boundary  $z=0$ , and by setting  $\theta_r = \theta_i$  :-

$$E_{io} + E_{ro} = E_{to} \quad (\text{y-component of E})$$

$$\left(\frac{E_{io}}{\eta_1} - \frac{E_{ro}}{\eta_1}\right) \cos\theta_i = \frac{E_{to}}{\eta_2} \cos\theta_t \quad (\text{x-component of H})$$

**Reflection coefficient**  $\Gamma_{\perp} = \frac{E_{ro}}{E_{io}} = \frac{\eta_2 \cos\theta_i - \eta_1 \cos\theta_t}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}$ ,  $E_{ro} = \Gamma_{\perp} E_{io}$

**Transmission coefficient**  $\tau_{\perp} = \frac{E_{to}}{E_{io}} = \frac{2\eta_2 \cos\theta_i}{\eta_2 \cos\theta_i + \eta_1 \cos\theta_t}$ ,  $E_{to} = \tau_{\perp} E_{io}$

where  $1 + \Gamma_{\perp} = \tau_{\perp}$

### Perpendicular Polarization - Brewster angle

- For no reflection (total transmission):

By setting  $\theta_i = \theta_{B\perp}$  :-

$$\Gamma_{\perp} = \frac{\eta_2 \cos \theta_{B\perp} - \eta_1 \cos \theta_i}{\eta_2 \cos \theta_{B\perp} + \eta_1 \cos \theta_i} = 0$$

$$\rightarrow \eta_2 \cos \theta_{B\perp} = \eta_1 \cos \theta_i$$

or

$$\eta_2^2 (1 - \sin^2 \theta_{B\perp}) = \eta_1^2 (1 - \sin^2 \theta_i)$$

$$\text{Since } \frac{\sin \theta_i}{\sin \theta_t} = \sqrt{\frac{\mu_1 \epsilon_1}{\mu_2 \epsilon_2}}, \text{ and } \theta_i = \theta_{B\perp}$$

$$\rightarrow \sin^2 \theta_{B\perp} = \frac{1 - (\epsilon_2 \mu_1 / \epsilon_1 \mu_2)}{1 - (\mu_1 / \mu_2)^2}$$

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### Summary

Property	Normal Incidence	Perpendicular	Parallel
Reflection coefficient	$\Gamma = \frac{\eta_2 - \eta_1}{\eta_2 + \eta_1}$	$\Gamma_{\perp} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$	$\Gamma_{\parallel} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$
Transmission coefficient	$\tau = \frac{2\eta_2}{\eta_2 + \eta_1}$	$\tau_{\perp} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$	$\tau_{\parallel} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$
Relation	$\tau = 1 + \Gamma$	$\tau_{\perp} = 1 + \Gamma_{\perp}$	$\tau_{\parallel} = (1 + \Gamma_{\parallel}) \frac{\cos \theta_i}{\cos \theta_t}$

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### Example 10.10

An EM wave travels in free space with the electric field component

$$\mathbf{E}_s = 100e^{j(0.866y+0.5z)} \mathbf{a}_x \text{ V/m}$$

Determine

- $\omega$  and  $\lambda$
- The magnetic field component
- The time average power in the wave

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### Example 10.10 -solution

- Comparing the given E with

$$\mathbf{E}_s = \mathbf{E}_0 e^{j\mathbf{k}\cdot\mathbf{r}} = E_0 e^{j(k_x x + k_y y + k_z z)} \mathbf{a}_x$$

it is clear that

$$k_x = 0, \quad k_y = 0.866, \quad k_z = 0.5$$

$$k = \sqrt{k_x^2 + k_y^2 + k_z^2} = \sqrt{(0.866)^2 + (0.5)^2} = 1$$

But in free space,

$$k = \beta = \omega \sqrt{\mu_0 \epsilon_0} = \frac{\omega}{c} = \frac{2\pi}{\lambda}$$

Hence,  $\omega = kc = 3 \times 10^8 \text{ rad/s}$

$$\lambda = \frac{2\pi}{k} = 2\pi = 6.283 \text{ m}$$

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**Example 10.10 - solution**

(b) the corresponding magnetic field is given by  $\mathbf{H}_s = \frac{\mathbf{a}_k \times \mathbf{E}_s}{\eta}$

$$\mathbf{a}_k = \frac{0.866\mathbf{a}_y + 0.5\mathbf{a}_z}{\sqrt{0.866^2 + 0.5^2}} = 0.866\mathbf{a}_y + 0.5\mathbf{a}_z$$

$$\mathbf{H}_s = \frac{0.866\mathbf{a}_y + 0.5\mathbf{a}_z}{\eta} \times 100\mathbf{a}_x e^{j(0.866y + 0.5z)}; \eta = (120\pi)$$

$$\mathbf{H}_s = (0.132\mathbf{a}_y - 0.23\mathbf{a}_z) e^{j(0.866y + 0.5z)} \text{ A/m}$$

(c) The time average power is

$$\begin{aligned} \phi_{avg} &= \frac{1}{2} \text{Re}(\mathbf{E}_s \times \mathbf{H}_s^*) = \frac{E_o^2}{2\eta} \mathbf{a}_k = \frac{(100)^2}{2(120\pi)} (0.866\mathbf{a}_y + 0.5\mathbf{a}_z) \\ &= 11.49\mathbf{a}_y + 6.631\mathbf{a}_z \text{ W/m}^2 \end{aligned}$$

**Example 10.11**

A uniform plane wave in air with

$$\mathbf{E} = 8 \cos(\omega t - 4x - 3z) \mathbf{a}_y \text{ V/m}$$

is incident on a dielectric slab ( $z \geq 0$ ) with  $\mu_r = 1$ ,  $\epsilon_r = 2.5$ ,  $\sigma = 0$ . Find

- The polarization of the wave
- The angle of incidence
- The reflected  $\mathbf{E}$  field
- The transmitted  $\mathbf{H}$  field

**Example 10.11 - solution**

(a) From the incident  $\mathbf{E}$  field, it is evident that the propagation vector is

$$\mathbf{k}_i = 4\mathbf{a}_x + 3\mathbf{a}_z \rightarrow k_i = 5 = \omega\sqrt{\mu_o\epsilon_o} = \frac{\omega}{c}$$

Hence,  $\omega = 5c = 15 \times 10^8 \text{ rad/s}$

A unit vector normal to the interface ( $z = 0$ ) is  $\mathbf{a}_z$ .

The plane containing  $\mathbf{k}$  and  $\mathbf{a}_z$  is  $y = \text{constant}$ , which is the  $xz$ -plane, the plane of incidence. Since  $\mathbf{E}_i$  is normal to this plane, we have perpendicular polarization (similar to Figure 10.17).

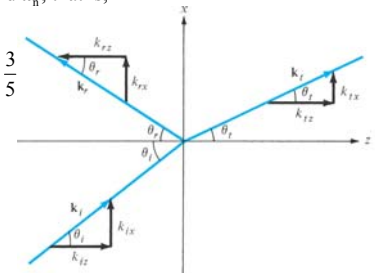
**Example 10.11 - solution**

(b) from the figure,  $\tan \theta_i = \frac{k_{ix}}{k_{iz}} = \frac{4}{3} \rightarrow \theta_i = 53.13^\circ$

Alternatively, we can obtain  $\theta_i$  from the fact that  $\theta_i$  is the angle between  $\mathbf{k}$  and  $\mathbf{a}_n$ , that is,

$$\begin{aligned} \cos \theta_i &= \mathbf{a}_k \cdot \mathbf{a}_n \\ &= \left( \frac{4\mathbf{a}_x + 3\mathbf{a}_z}{5} \right) \cdot \mathbf{a}_z = \frac{3}{5} \end{aligned}$$

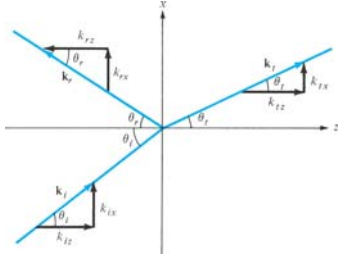
or  $\theta_i = 53.13^\circ$



**Example 10.11 - solution**

(c) Let  $E_r = E_{r0} \cos(\omega t - \mathbf{k}_r \cdot \mathbf{r}) \mathbf{a}_y$ , which is similar to form to the given  $E_i$ . The unit vector  $\mathbf{a}_y$  is chosen in view of the fact that the tangential component of  $\mathbf{E}$  must be continuous at the interface. From the Figure:

$\mathbf{k}_r = k_{rx} \mathbf{a}_x - k_{rz} \mathbf{a}_z$   
 $k_{rx} = k_r \sin \theta_r$ ,  $k_{rz} = k_r \cos \theta_r$   
 But  $\theta_r = \theta_i$  and  $k_r = k_i = 5$   
 because both  $k_r$  and  $k_i$  are in the same medium. Hence  
 $k_r = 4\mathbf{a}_x - 3\mathbf{a}_z$



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**Example 10.11 - solution**

To find  $E_{r0}$ , we need  $\theta_r$ . From Snell's law

$$\sin \theta_i = \frac{n_1}{n_2} \sin \theta_t = \frac{c\sqrt{\mu_1 \epsilon_1}}{c\sqrt{\mu_2 \epsilon_2}} \sin \theta_i = \frac{\sin 53.13^\circ}{\sqrt{2.5}}$$

or  $\theta_r = 30.39^\circ$

$$\Gamma_{\perp} = \frac{E_{r0}}{E_{i0}} = \frac{\eta_2 \cos \theta_i - \eta_1 \cos \theta_t}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

where  $\eta_1 = \eta_0 = 377$ ,  $\eta_2 = \sqrt{\frac{\mu_0 \mu_{r2}}{\epsilon_0 \epsilon_{r2}}} = \frac{377}{\sqrt{2.5}} = 238.4$

$$\Gamma_{\perp} = \frac{E_{r0}}{E_{i0}} = \frac{238.4 \cos 53.13^\circ - 377 \cos 30.39^\circ}{238.4 \cos 53.13^\circ + 377 \cos 30.39^\circ} = -0.389$$

Hence,  $E_{r0} = \Gamma_{\perp} E_{i0} = -0.389(8) = -3.112$

$\mathbf{E}_r = -3.112 \cos(15 \times 10^8 t - 4x + 3z) \mathbf{a}_y$  V/m

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**Example 10.11 - solution**

(d) Similarly, let the transmitted electric field be

$E_t = E_{t0} \cos(\omega t - \mathbf{k}_t \cdot \mathbf{r}) \mathbf{a}_y$

where  $k_t = \beta_2 = \omega \sqrt{\mu_2 \epsilon_2} = \frac{\omega}{c} \sqrt{\mu_{r2} \epsilon_{r2}} = \frac{15 \times 10^8}{3 \times 10^8} \sqrt{1 \times 2.5} = 7.906$

From the Figure,

$k_{tx} = k_t \sin \theta_t = 4$

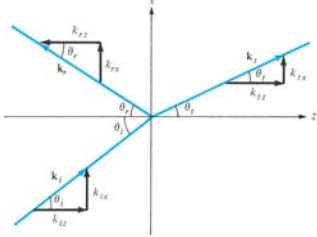
$k_{tz} = k_t \cos \theta_t = 6.819$

$\mathbf{k}_t = 4\mathbf{a}_x + 6.819\mathbf{a}_z$

Notice that  $k_{ix} = k_{rx} = k_{tx}$

$$\tau_{\perp} = \frac{E_{t0}}{E_{i0}} = \frac{2\eta_2 \cos \theta_i}{\eta_2 \cos \theta_i + \eta_1 \cos \theta_t}$$

$$= \frac{2 \times 238.4 \cos 53.13^\circ}{238.4 \cos 53.13^\circ + 377 \cos 30.39^\circ} = 0.611$$



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**Example 10.11 - solution**

The same result could be obtained from the relation  $\tau = 1 + \Gamma$ . Hence,

$E_{t0} = \tau_{\perp} E_{i0} = 0.611 \times 8 = 4.888$

$\mathbf{E}_t = 4.888 \cos(15 \times 10^8 t - 4x - 6.819z) \mathbf{a}_y$

From  $\mathbf{E}_t$ ,  $\mathbf{H}_t$  is easily obtained as

$$\mathbf{H}_t = \frac{\mathbf{a}_{k_t} \times \mathbf{E}_t}{\eta_2} = \frac{4\mathbf{a}_x + 6.819\mathbf{a}_z}{7.906(238.4)} \times 4.888 \mathbf{a}_y \cos(\omega t - \mathbf{k}_t \cdot \mathbf{r})$$

$\mathbf{H}_t = (-17.69\mathbf{a}_x + 10.37\mathbf{a}_z) \cos(15 \times 10^8 t - 4x - 6.819z)$  mA/m