Building Materials Laboratory Manual

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2010/2009
How to write a laboratory report

The following arrangement of the report is suggested:

**Title**  This should indicate the nature of the test and the specifications number used.

**Scope of the test:**  A brief statement of the purpose and significance of the test should be indicated.

**Materials:**  The materials used or tested should be described.

**Apparatus and method of testing:**  Special equipment used should be briefly described. The testing procedure should be also described.

**Data and results of the test:**  All laboratory data shall be submitted in tabular form. Observations relating to the behavior of the materials should be included. All equations or formulas used should be clearly indicated. Calculations should be properly checked. The results of the test should be summarized in tabular or graphical form.

**Discussion**  There should be included a brief discussion in which attention is drawn to the silent facts shown by the tables and diagrams. The test results should be compared with the standard values and conclusion should be drawn.
Reducing Field Sample of Aggregate to Test Sample
ASTM C 702, D75

**Purpose:** To obtain laboratory samples of aggregates from stockpiles.

**Equipment:** Shovel, scoop, boom.

**Procedure:**
1- Obtain a sample of aggregate (about 50 kg) from three places in the stockpile: from the top third, at the midpoint, and from the bottom third of the volume of the pile.
2- Place the field sample on a hard, clean level surface.
3- Mix the material thoroughly by turning the entire sample three times.
4- Shovel the entire sample into a conical pile.
5- Carefully flatten the conical to a uniform thickness and diameter by pressing down the apex with a shovel. (The diameter should be approximately four to eight times the thickness).
6- Divide the flattened mass into four equal quarters with a shovel.
7- Remove two diagonally opposite quarters. Brush the cleared spaces clean.
8- Mix and quarter the remaining materials until the sample is reduced to the desired size.

**Note**
The sample splitters can be used instead of flattening the mass on a level surface.
Fig. (1) The sample splitters for fine & coarse aggregates

Fig. (2) Reducing Field Sample of Aggregate to Test Sample
Test No.1:

“Moisture Content of Concrete Aggregate”
( ASTM C-566-84)

Scope of test:
One of the properties of the aggregates which should be known to design a concrete mix is its moisture content. It is necessary in order to determine the net water-cement ratio in a batch of concrete made with job aggregate.

Materials:
The amount of materials depends on the nominal maximum size of aggregate as follows:

<table>
<thead>
<tr>
<th>N.M.S (mm)</th>
<th>Weight of Sample (kg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>4.75</td>
<td>0.5</td>
</tr>
<tr>
<td>9.5</td>
<td>1.5</td>
</tr>
<tr>
<td>12.5</td>
<td>2</td>
</tr>
<tr>
<td>19</td>
<td>3</td>
</tr>
<tr>
<td>25</td>
<td>4</td>
</tr>
<tr>
<td>37.5</td>
<td>6</td>
</tr>
</tbody>
</table>

Apparatus:
1. A balance sensitive to 0.5gm.
2. Electrical oven at temperature 105 °C.
3. Container with a cover.
4. Sample splitter.

Procedure:
1- Prepare the container clean, record its empty weight (A).
2- Weigh the suitable sample of aggregate and keep it in a container, put the cover on.
3- The weight of the container with the cover and the gravel is (B).
4- Remove the cover, then put the sample in the oven at 105 °C for 24 hours.
5- Remove the sample forms the oven and put the cover on it, then leaves it for half

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an hour, and then weigh it (D).
6- Repeat the same steps for the sand sample.

**Calculations and Results:**

\[
\text{Moisture Content } \% = \left[ \frac{B - D}{D - A} \right] \times 100
\]

**Discussion:**
1- Comment on the results you get.
2- Do you think that your results are affected by the weather conditions?
Test 2:

“Specific Gravity and Absorption of Coarse Aggregate”
(\textit{ASTM C 127 – 88})

\textbf{Scope:}

This test method covers the determination of Specific Gravity and Absorption of coarse aggregate. The specific gravity may be expressed as bulk specific gravity, bulk specific gravity SSD or apparent specific gravity. The bulk specific gravity and absorption are based on aggregate after 24 hour soaking in water.

\textbf{Materials:}

1- Coarse aggregate, must be sampled using sample splitter.
2- The weight of the sample depends on nominal maximum size (NMS) of the aggregate as follows.

<table>
<thead>
<tr>
<th>N.M.S (mm)</th>
<th>Minimum Weight of Sample (kg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>12.5 or less</td>
<td>2</td>
</tr>
<tr>
<td>19</td>
<td>3</td>
</tr>
<tr>
<td>25</td>
<td>4</td>
</tr>
<tr>
<td>37.5</td>
<td>5</td>
</tr>
<tr>
<td>50</td>
<td>8</td>
</tr>
</tbody>
</table>

\textbf{Apparatus:}

1- A weighing balance sensitive, readable and accurate to 0.5gm.
2- The balance shall be equipped with suitable apparatus for suspending the sample container in water.
3. Sample container (A wire basket) [20cm diameter & 20cm in height].
4. Water tank; a watertight tank into which the sample container may be placed while suspended below the balance.
5- Sieves; 4.75mm (No.4) or other sizes as needed

\textbf{Procedure:}

1- Take the sample of coarse aggregate using the sample splitter.
2- Sieve the sample with 4.75mm sieves and ignore the materials passing through No.4.75 sieve.
3- Wash the sample to remove dust.
4- Put the sample in the oven at 105°C for 24 hours.
5- Get the sample out of the oven, leave it to cool then determine its weight.
6- Submerge the sample in water for 24 hours.

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7- Remove the sample from the water and roll it in a large absorbent cloth until all visible films of water are removed. Wipe the larger particles individually. Take care to avoid evaporation of water from aggregate pores during the operation of surface-drying.
8- Take the required weight of the sample in its (S.S.D) (saturated surface dry) condition.
9- After weighing, immediately place the S.S.D sample in the sample container and determine its weight in water at 23±1°C. Take care to remove all entrapped air before weighing by shaking the container while immersed.
10- Dry the test sample to constant weight at a temperature of 110±5°C, Cool in air at room temperature 1 to 3 hours, or until the aggregate has cooled to a temperature that is comfortable to handle, and weigh.

Calculations :-

1-Specific Gravity:-

a. Bulk specific gravity: - Calculate the bulk specific gravity as follows:

Bulk Specific Gravity = A / (B-C)

Where:
A = Weight of oven-dry test sample in air, (gm).
B = Weight of S.S.D. sample in air, (gm).
C = Weight of saturated sample in water, (gm).

b- Bulk Specific Gravity (SSD) = B / (B-C)

c- Apparent Specific gravity: - Calculate the apparent sp. gr. As follows:

Apparent Specific Gravity = A / (A - C)

2- Absorption:-

Calculate the percentage of absorption as follows:

Absorption% = [(B - A) / A ] x 100

Discussion:
1- Comment on the results.
2- Compare the results with the typical values.
3- How can the percentage of absorption affect on a concrete mix?
Fig.(3) A balance with suitable apparatus for suspending the sample container in water.
Test No.3

“Specific Gravity and Absorption of fine Aggregate”

(ASTM C 127 – 88)

Scope: This test method covers the determination of Bulk and Apparent Specific Gravity and Absorption of fine aggregate.

Materials: - 1 kg of sand is used using sample splitter.

Apparatus:

1- A balance having capacity of 1kg or more sensitive to 0.1gm
2- Pycnometer: A flask or other suitable container into which the fine aggregate sample can be introduced. It is usually of 500cm$^3$ capacity.
3- Mold: a metal mold in the form of a frustum of a cone with dimensions as follows: 37mm inside diameter at the top, 90mm inside diameter at the bottom and 75mm in height.
4- Tamper: A metal tamper weighing 340±15gm and having a flat circular tamping face 25mm in diameter.
5- Electrical Oven.
6- A container suitable to submerge the sample with water.

Preparation of the test Specimen:

1- Obtain approximately 1kg of the fine aggregate using sample splitter.
2- Dry it in a suitable pan or vessel to constant weight at 110°C. Allow it to cool to a comfortable handling temperature, cover with water by immersion and permit to stand for 24 hours.
3- Decant excess water with care to avoid loss of fines, spread the sample on a flat nonabsorbent surface exposed to a gently moving current of warm air.
4- Stir frequently to get homogeneous drying until achieving the saturated surface dry condition. Use cone test for surface moisture.
5- Hold the mold firmly on a smooth nonabsorbent surface with the large diameter down. Place a portion of partially dried fine aggregate loosely in the mold by filling it to over following and heaping additional materials above the top of the mold.
6- Lightly tamp the sand into the mold with 25 light drops of the tamper. Each drop should start about 5mm above the top surface of the sand. Permit the tamper to fall freely under gravitational attraction on each drop.
7- Adjust the surface, remove loose sand from the base and lift the mold vertically. If surface moisture is still present the sand will retain the molded shape. When the sand slumps slightly, it indicates that it has reached S.S.D condition.
Procedure:

1. Weigh 500gm of the S.S.D sample.
2. Partially fill the pycnometer with water. Immediately put the pycnometer 500gm saturated surface dry aggregate.
3. Then fill with additional water to approximately 90% of capacity.
4. Roll; invert the pycnometer to eliminate all air bubbles.
5. Adjust its temperature to 23±1.7 °C by putting the pycnometer in a water bath for an hour.
6. Bring the water level in the pycnometer to its calibrated capacity.
7. Determine the total weight of the pycnometer, specimen and water.
8. Remove the fine aggregate from the pycnometer, dry to constant weight at temp. 110±5 C, cool in air at room temperature for one hour, and weigh.
9. Determine the weight of the pycnometer filled to its capacity with water at 23 °C

Calculations:

1. Calculate the bulk specific gravity as follows:

   \[ \text{Bulk sp. gr.} = \frac{A}{B + S - C} \]

   Where: 
   - A: Weight of oven — dry specimen in air, (gm).
   - B: Weight of pycnometer filled with water, (gm)
   - S: Weight of the saturated surface-dry specimen. (500 gm)
   - C: Weight of pycnometer with specimen and water to calibration mark, (gm).

2. Calculate the bulk specific gravity (SSD) as follows:

   \[ \text{Bulk sp. gr. (SSD)} = \frac{S}{B + S - C} \]

3. Calculate the apparent Specific Gravity as follows:

   \[ \text{Apparent sp. gr} = \frac{A}{B + A - C} \]

3. Calculate the percentage of absorption as follows:

   \[ \text{Absorption} = \left[ \frac{S - A}{A} \right] \times 100 \]

Discussion:

1. Comment on the results.
2. Compare the results with the typical values.
3. How can the percentage of absorption affect on a concrete mix?
Fig.(4) Exposing the fine aggregate to a gently moving current of warm air.

Fig.(5) The fine aggregate is still damp.

Fig.(6) The fine aggregate is in SSD condition.
Test No.4

“Resistance to Degradation of Small-size coarse Aggregate by Abrasion in the Los Angeles Machine.”

ASTM C 131-81(1987)

Scope of test: This test method cover testing sizes of coarse of (12.5mm) for resistance to degradation using the Los Angeles testing machine.

Summary of test:

The Los Angeles test is a measure of degradation of mineral aggregates of standard grading resulting form a combination of actions including abrasion or attrition, impact, and grinding in a rotating steel drum containing a specified number of steel spheres, the number depending upon the grading of the test sample. As the drum rotates a shelf plate picks up the sample and the steel spheres, carrying them around until they are dropped to the opposite side of the drum, creating an impact-crushing effect. The contents then roll within the drum with an abrading and grinding action until the shelf plate impacts and the cycle is repeated. After the prescribed number of revolutions, the content is removed from the drum and the aggregate portion is sieved to measure the degradation as percent loss.

Materials:

The test sample shall be washed and oven-dried at (105-110) °C and separated into individual size fractions and recombined to the grading of table (1) most nearly corresponding to the range of sizes in the aggregate as furnished for the work.

Apparatus:-
1. Los Angeles Machine.
2. Sieves.
3. Balance accurate to 0.5 gm.
4. Oven. And containers.
5. Charge – The Charge must consist of steel spheres averaging (46.8mm) in diameter and each weighing between 390 to 445 gm. The charge, depending upon the grading of the test sample as follows:
Grading | No: of spheres | Wt of charge (gm)
---|---|---
A | 12 | 5000±25
B | 11 | 4584±25
C | 8 | 3330±20
D | 6 | 2500±15

**Procedure:**

1. Put the sample of coarse aggregate in an oven at 105°C to get oven-dry sample.
2. Prepare the sample, then Weigh and record its weight to the nearest 1 gm.
3. Place the test sample and charge in the Los Angeles testing machine and rotate the machine at 30 to 33 round/mm for 500 revolutions.
4. Discharge the material from the machine and make preliminary separation of the sample as sieve coarser than (1.7mm). The finer portion shall then be sieved on a 1.7mm sieve.
5. The material coarser than the 1.7mm sieve shall be washed, oven dried at 105°C to substantially constant weight, and weighed to the nearest 5 gm.

**Calculations:**

\[
\% \text{Abrasion} = \frac{\text{wt of initial sample} - \text{wt of retained of 1.7mm sieve}}{\text{wt of initial sample}} \times 100
\]

Or \[
= \frac{\text{wt of passing sieve (1.7mm)}}{\text{wt. of initial sample}} \times 100
\]

**Note:**

ASTM Specifications C33-86 requires that the abrasion percent should not exceed 50% for coarse aggregate used in concrete mixes.

Prepared by: B. J. Farid
Table (1): Grading of test samples:

<table>
<thead>
<tr>
<th>Sieve size (mm)</th>
<th>Retained on</th>
<th>Weight of indicated sizes (gm)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>A</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Grading</td>
</tr>
<tr>
<td>37.5</td>
<td>25</td>
<td>1250+25</td>
</tr>
<tr>
<td>25</td>
<td>19</td>
<td>1250+25</td>
</tr>
<tr>
<td>19</td>
<td>12.5</td>
<td>1250+10</td>
</tr>
<tr>
<td>12.5</td>
<td>9.5</td>
<td>1250+10</td>
</tr>
<tr>
<td>9.5</td>
<td>6.3</td>
<td>-</td>
</tr>
<tr>
<td>6.3</td>
<td>4.75</td>
<td>-</td>
</tr>
<tr>
<td>4.75</td>
<td>2.36</td>
<td>-</td>
</tr>
<tr>
<td>Total</td>
<td></td>
<td>5000+10</td>
</tr>
</tbody>
</table>

Fig. (7) The Los Angeles Machine.
AGGREGATE CRUSHING STRENGTH TEST

Theory and Scope:
This is one of the major Mechanical properties required in a road stone. The test evaluates the ability of the Aggregates used in road construction to withstand the stresses induced by moving vehicles in the form of crushing. With this, the aggregates should also provide sufficient resistance to crushing under the roller during construction and under rigid tyre rims of heavily loaded animal drawn vehicles.

The crushing strength or aggregate crushing value of a given road aggregate is found out as per IS-2386 Part-4.

The aggregate crushing value provides a relative measure of resistance to crushing under a gradually applied compressive load. To achieve a high quality of pavement aggregate possessing low aggregate crushing value should be preferred.

The aggregate crushing value of the coarse aggregates used for cement concrete pavement at surface should not exceed 30% and aggregates used for concrete other than for wearing surfaces, shall not exceed 45% as specified by Indian Standard (IS) and Indian Road Congress (IRC).

Aim: To determine crushing strength of a given aggregate as per IS: 2386 part - IV

Apparatus:
/. A steel cylinder of internal diameter 15.2 cm (Steel cylinder with open ends).
/. A square base plate, plunger having a piston diameter of 15 cm.
/. A cylindrical measure of internal diameter of 11.5 and height 18 cms.
/. Steel tamping rod having diameter of 1.6 cms length 45 to 60 cms.
/. Balance of capacity 3 kg with accuracy up to 1 gm.
/. Compression testing machine capable of applying load of 40 tonnes at a loading rate of 4 tonnes per minute
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**Procedure:**

~ The aggregate in surface-dry condition before testing and passing 12.5 mm sieve and retained on 10 mm sieve is selected.

~ The cylindrical measure is filled by the test sample of the aggregate in three layers of approximately equal depth, each layer being tamped 25 times by the rounded end of the tamping rod.

~ After the third layer is tamped, the aggregates at the top of the cylindrical measure are leveled off by using the tamping rod as a straight edge. Then the test sample is weighed. Let that be WI gm.

~ Then the cylinder of test apparatus is kept on the base plate and one third of the sample from cylindrical measure is transferred into cylinder and tamped 25 times by rounded end of the tamping rod.

~ Similarly aggregate in three layers of approximately equal depth, each layer being tamped 25 times by rounded end of the tamping rod.

~ Then the cylinder with test sample and plunger in position is placed on compression testing machine.

~ Load is then applied through the plunger at a uniform rate of 4 tonnes per minute until the total load is 40 tonnes and the load is released.

~ Aggregates including the crushed position are removed from the cylinder and sieved on a 2.36mm IS. sieve and material which passes this sieve is collected and weighed. Let this be W2 gm.

~ The above step is repeated with second sample of the same aggregate. The two tests are made for the same specimen for taking an average value.

~ Total weight of dry sample taken is WI gm weight of the portion of crushed material passing 2.36mm IS sieve be W2 gm.

Then the aggregate crushing value is defined as the ratio of weight of fines passing the specified IS sieve to the total weight of the sample (WI).

Aggregate crushing value = 100*W2/WI%
Aggregate Crushing Test Apparatus

Crushing Test in Progress
Observation and Calculation:

<table>
<thead>
<tr>
<th>Average aggregate crushing strength value</th>
<th>Aggregate crushing value %</th>
<th>Weight of fines passing 2.36mm IS sieve, w2gm</th>
<th>Total weight of dry aggregate sample 10 gm</th>
<th>Trials</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>2</td>
</tr>
</tbody>
</table>

Aggregate crushing value = 100*W2/W1.

Result:

The mean (average) of the crushing value aggregate is ________________________ %

Viva voce:

1. What do you understand by the term "Ten percent Fines value"?
2. Define aggregate crushing value and how crushing strength test is carried out on cylindrical stone specimen explain.

3. What is the use or application of the aggregate crushing test?

**Reference:**


3. Indian Standard Specifications for Coarse and Fine Aggregate from Natural Sources for Concrete, IS: 383 Indian Standards Institution.

ABRASION TEST

Theory and Scope:
Abrasion is a measure of resistance to wear or hardness. It is an essentially property for road aggregates especially when used in wearing coarse. Due to the movements of traffic, the road stones used in the surfacing course are subjected to wearing actions at the top. When traffic moves on the road the soil particle (sand) which comes between the wheel and road surface causes abrasion on the road stone. The abrasion test on aggregate is found as per I.S.-2386 part-IV.

Abrasion tests on aggregates are generally carried out by anyone of the following methods:
1. Los Angeles abrasion test.
2. Deval abrasion test.
3. Dorry abrasion test.

Los Angeles Abrasion Test: - The principle of Los Angeles abrasion test is to find the percentage wear due to the relative rubbing action between the aggregates and steel balls used as abrasive charge pounding action of these balls also exist while conducting the test. Maximum Allowable Los Angeles Abrasion Values of Aggregates in Different types of pavement layers as per Indian Road Congress (IRC) are:-

For sub-base course a value of 60%. For base course such as WBM, Bituminous Macadam (B.M.), Built-Up spray grout base course and etc. value of 50%.

For surface course such as WBM, BM, Bituminous Penetration Macadam, Built-Up spray grout binder course and etc. a value of 40%.

If aggregates are used in surface course as Bituminous carpet, Bituminous surface dressing, single or two coats, cement concrete surface coarse and etc. a value of 35%.
If aggregates are used for Bituminous concrete, Cement concrete pavement as surface coarse than aggregate abrasion value of 30% maximum.

**Aim:** To determine the abrasion value of given aggregate sample by conducting Los Angeles abrasion Test.

**Apparatus:**

- 1/ A Los Angeles machine with inside diameter 70cm and inside length of 50%. Abrasive charges.
- 1/ A LS Sieve with 1.7mm opening.
- 1/ A Weighting Balance of 0.1gm accuracy.

**Procedure:**

- Clean and dry aggregate sample confirming to one of the grading A to G is used for the test. (Refer table no. 1)
- Aggregates weighing 5Kg for grading A, B, C or D and 10Kg for gradings E, F or G may be taken as test specimen and placed in the cylinder.
- The abrasive charge is also chosen in accordance with table no. 1 and placed in the cylinder of the machine, and cover is fixed to make dust tight.
- The machine is rotated at a speed of 30 to 33 revolutions per minute.
- The machine is rotated for 500 revolutions for gradings A, B, C and D, for gradings E, F and G, it shall be rotated for 1000 revolutions.
- After the desired number of revolutions, the machine is stopped and the material is discharged from the machine taking care to take out entire stone dust.
- Using a sieve of size larger than 1.70mm LS sieve, the material is first separated into two parts and the finer position is taken out and sieved further on a 1.7mm LS sieve.
- Let the original weight of aggregate be W1gm, weight of aggregate retained on 1.70mm LS sieve after the test be W2gm.
Los Angeles abrasion value \( \% = \frac{1 - \frac{W}{w}}{2} \times 100 \).

Schematic Diagram of Los Angeles Abrasion Testing Machine

Los Angeles Abrasion Testing Machine
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## Observation and Calculation:

<table>
<thead>
<tr>
<th>Sl. No.</th>
<th>Details of Sample</th>
<th>Trail 2</th>
<th>Trail 1</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>Weight of Specimen = WIg</td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>Weight of Specimen after abrasion test, coarser than 70 mm IS sieve = W2 g</td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>Percentage wear = [(WI - W2) / WI] * 100</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>
### TABLE NO.1

<table>
<thead>
<tr>
<th>Abrasive Charge.</th>
<th>Weight in grams of each test sample in the size range, mm (passing and retained on Square holes)</th>
<th>~</th>
<th>~</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>4.75-2.36</td>
<td>6.3-4.75</td>
<td>10-6.3</td>
</tr>
<tr>
<td>Weight of charge, g</td>
<td>No. of Spheres</td>
<td></td>
<td></td>
</tr>
<tr>
<td>5000± 25</td>
<td>12</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>4584± 25</td>
<td>11</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>3330± 20</td>
<td>8</td>
<td>-</td>
<td>2500</td>
</tr>
<tr>
<td>2500± 15</td>
<td>6</td>
<td>5000</td>
<td>-</td>
</tr>
<tr>
<td>5000± 25</td>
<td>12</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>5000± 25</td>
<td>12</td>
<td>-</td>
<td>-</td>
</tr>
<tr>
<td>5000± 25</td>
<td>12</td>
<td>-</td>
<td>-</td>
</tr>
</tbody>
</table>
Result:
The average value of two Los Angeles abrasion test is _______________%

Viva voce:
1. The abrasion value found from Los Angeles test for two aggregates A and B are 50% and 38% respectively. Which aggregate is harder? Why? For what types of constructions are these suitable?
2. Why Los Angeles abrasion test is considered superior to the other form of tests which are used to determine the hardness of aggregates?
3. Two materials have abrasion values 3 and 10 respectively. Which one is harder and why?

Reference:
2. Indian Standard Specifications for Coarse and Fine Aggregate from Natural Sources for Concrete, IS: 383 Indian Standards Institution.
**IMPACT TEST**

**Theory and Scope:**

Toughness is the property of a material to easiest impact. Due to moving loads the aggregates are subjected to pounding action or impact and there is possibility of stones breaking into smaller pieces. Therefore a test designed to evaluate the toughness of stones i.e., the resistance of the stones to fracture under repeated impacts may be called Impact test on aggregates. The test can also be carried on cylindrical stone specimen known as Page Impact test. The aggregate Impact test has been standardized by Indian Standard Institution. The aggregate impact test is conducted as per IS-2386 Part IV.

The aggregate Impact value indicates a relative measure of the resistance of aggregate to a sudden shock or an Impact, which in some aggregates differs from its resistance to a slope compressive load in crushing test. A modified Impact test is also often carried out in the case of soft aggregates to find the wet Impact value after soaking the test sample.

Various agencies have specified the maximum permissible aggregate Impact values for the different types of pavements. IRC has specified the following values.

The maximum allowable aggregate Impact value for water bound Macadam; Sub-Base coarse 50% where as cement concrete used in base course is 45%. WBM base course with Bitumen surface in should be 40%. Bituminous Macadam base course should have A.I.V of 35%. All the surface courses should possess an A.I.V below 30%.

**Aim:** To determine the aggregate impact value of given aggregate as per IS-2386 Part IV.

**Apparatus:** The apparatus consists of an Impact testing machine: The machine consists of a metal base. A detachable cylindrical steel cup of internal diameter 10.2cm and depth 5cm. A metal hammer of weight between 13.5 to 14Kg, 10cm in diameter and 5cm long. An arrangement for raising the hammer and allow it to fall freely between vertical guides from a height of 38cm on the test sample in the cup.
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A cylindrical metal measure having 7.5 cm and depth of 5 cm for measuring aggregates.

A tamping rod of circular cross section, 1 cm in diameter and 23 cm long, rounded at one end.

I.S. sieve of sizes 12.5 mm, 10 mm and 2.36 mm.

Balance of capacity not less than 500 gm to weigh accurate up to 0.01 gm.

**Procedure:**

- The test sample consists of aggregates passing 12.5 mm sieve and retained on 10 mm sieve and dried in an oven for 4 hours at a temperature of 100°C to 110°C.
- The aggregates are filled up to about 1/3 full in the cylindrical measure and tamped 25 times with rounded end of the tamping rod.
- The rest of the cylindrical measure is filled by two layers and each layer being tamped 25 times.
- The overflow of aggregates in the cylindrical measure is cut off by tamping rod using it has a straight edge.
- Then the entire aggregate sample in a measuring cylinder is weighted nearing to 0.01 gm.
- The aggregates from the cylindrical measure are carefully transferred into the cup which is firmly fixed in position on the base plate of the machine. Then it is tamped 25 times.
- The hammer is raised until its lower face is 38 cm above the upper surface of aggregates in the cup and allowed to fall freely on the aggregates. The test sample is subjected to a total of 15 such blows each being delivered at an interval of not less than one second. The crushed aggregate is then removed from the cup and the whole of it is sieved on 2.36 mm sieve until no significant amount passes. The fraction passing the sieve is weighed accurate to 0.1 gm. Repeat the above steps with other fresh sample.
Let the original weight of the oven dry sample be $W_{1}\text{gm}$ and the weight of fraction passing 2.36mm I.S sieve be $W_2\text{gm}$. Then aggregate Impact value is expressed as the $\%$ of fines formed in terms of the total weight of the sample.

$$\text{Aggregate Impact Value} = \frac{100 \times W_2}{W_1} \%.$$
## Concrete and Highway Materials Testing Laboratory

### Details of Sample

<table>
<thead>
<tr>
<th>Average</th>
<th>Trail 2</th>
<th>Trail 1</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>Details of Sample</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Sl. No.</td>
</tr>
<tr>
<td></td>
<td></td>
<td>1</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Total Weight of aggregate sample filling the cylinder measure = $W_1g$</td>
</tr>
<tr>
<td></td>
<td></td>
<td>2</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Weight of aggregate passing 2.36 mm sieve after the test = $W_2g$</td>
</tr>
<tr>
<td></td>
<td></td>
<td>3</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Weight of aggregate retained 2.36 mm sieve after the test = $W_2g$</td>
</tr>
<tr>
<td></td>
<td></td>
<td>4</td>
</tr>
<tr>
<td></td>
<td></td>
<td>$(W1 - W_2 + W_3)$</td>
</tr>
<tr>
<td></td>
<td></td>
<td>5</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Aggregate Impact Value = $(W_2/W_1) \times 100$ Percent</td>
</tr>
</tbody>
</table>

### Result:

The mean A.I.V is %.  

### Viva voce:

1. How is aggregate Impact expressed?
2. What do you understand by dry and wet Impact value?
3. Aggregate Impact value of material A is 15 and that of B is 35. Which one is better for surface course?

### Reference:

2. Indian Standard Specifications for Coarse and Fine Aggregate from Natural Sources for Concrete, IS: 383 Indian Standards Institution.
SHAPE TEST (Flakiness Index)

Theory and Scope:
The particle shape of aggregate is determined by the percentages of flaky and elongated particles contained in it. In case of gravel it is determined by its Angularity Number. Flakiness and Elongation tests are conducted on coarse aggregates to assess the shape of aggregates. Aggregates which are flaky or elongated are detrimental to the higher workability and stability of mixes. They are not conducive to good interlocking and hence the mixes with an excess of such particles are difficult to compact to the required degree. For base coarse and construction of bituminous and cement concrete types, the presence of flaky and elongated particles are considered undesirable as they may cause inherent weakness with probabilities of breaking down under heavy loads. Rounded aggregates are preferred in cement concrete road construction as the workability of concrete improves. Angular shape of particles are desirable for granular base coarse due to increased stability derived from the better interlocking when the shape of aggregates deviates more from the spherical shape, as in the case of angular, flaky and elongated aggregates, the void content in an aggregate of any specified size increases and hence the grain size distribution of the graded aggregates has to be suitably altered in order to obtain minimum voids in the dry mix or the highest dry density. It is determined according to the procedure laid down in IS-2386 (PART-I).

FLAKINESS INDEX: The flakiness index of aggregates is the percentage by particles whose least dimension (thickness) is less than $3/S^{th}$ (0.6) of their mean dimension. The test is not applicable to sizes smaller than 6.3mm.

ELONGATION INDEX: The elongation index of an aggregate is the percentage by weight of particles whose greatest dimension (length) is greater than 1 and $4/S^{th}$ times (1.8 times) their mean dimensions. The elongation test is not applicable to sizes smaller than 6.3mm.
**ANGULARITY NUMBER:** The angularity number of an aggregate is the amount by which the percentage voids exceeds 33 after being compacted in a prescribed manner. The minimum allowable combined index of aggregates used in surface course in different types of pavement is 30%.

**Aim:** To determine the flakiness Index of a given aggregates sample.

**Apparatus:** The apparatus consists of a standard thickness gauge, I.S. sieves of sizes 63, 50, 40, 31.5, 25, 20, 16, 12.5, 10 and 6.3mm and a balance to weigh the samples.

**Procedure:**

~ The sample is sieved with the sieves mentioned in the table.
~ A minimum of 200 pieces of each fraction to be tested are taken and weighed (wlgm).

~ In order to separate flaky materials, each fraction is then gauged for thickness on thickness gauge, or in bulk on sieve having elongated slots as specified in the table.
~ Then the amount of flaky material passing the gauge is weighed to an accuracy of atleast 0.1 % of test sample.
~ Let the weight of the flaky materials passing the gauge be wlgm. Similarly the weights of the fractions passing and retained on the specified sieves be w1, w2, w3, etc. are weighed and the total weight w1+w2+w3+ ... = wg is found. Also the weights of the materials passing each of the specified thickness gauge are found = W1, W2, W3 ... and the total weight of the material passing the different thickness gauges = W1+W2+W3+ ... =Wg is found.
~ Then the flakiness index is the total weight of the flaky material passing the various thickness gauges expressed as a percentage of the total weight of the sample gauged

\[
\text{Flakiness Index} = \left( \frac{w}{W + w_1 + w_2 + \ldots} \right) 100
\]
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Thickness Gauge

Flakiness Index Test in Progress
Observation and Calculation:

<table>
<thead>
<tr>
<th>Weight of aggregates in each fraction passing thickness gauge, gm.</th>
<th>Weight of the fraction consisting of at least 200 pieces in gm.</th>
<th>THICKNESS GAUGE (0.6 TIMES THE MEAN SIEVE) mm</th>
<th>SIZE OF AGGREGATE</th>
</tr>
</thead>
<tbody>
<tr>
<td>33.90</td>
<td>50</td>
<td>63</td>
<td></td>
</tr>
<tr>
<td>27.00</td>
<td>40</td>
<td>50</td>
<td></td>
</tr>
<tr>
<td>19.50</td>
<td>25</td>
<td>40</td>
<td></td>
</tr>
<tr>
<td>16.95</td>
<td>25</td>
<td>31.5</td>
<td></td>
</tr>
<tr>
<td>13.50</td>
<td>20</td>
<td>25</td>
<td></td>
</tr>
<tr>
<td>10.80</td>
<td>16</td>
<td>20</td>
<td></td>
</tr>
<tr>
<td>8.55</td>
<td>12.5</td>
<td>16</td>
<td></td>
</tr>
<tr>
<td>6.75</td>
<td>10.0</td>
<td>12.5</td>
<td></td>
</tr>
<tr>
<td>4.89</td>
<td>6.3</td>
<td>10</td>
<td></td>
</tr>
</tbody>
</table>

Result: The flakiness index of the given sample of aggregates is _____________ %. 
SHAPE TEST (Elongation Index)

**Aim:** To determine the Elongation Index of the given aggregate sample.

**Apparatus:** Length gauge, I.S-sieves as given in the table and a balance of accuracy 0.01 Gm.

**Procedure:**

~ The sample is sieved through I. S-sieves specified in the table. A minimum of 200 aggregate pieces of each fraction is taken and weighed.

~ Each fraction is thus gauged individually for length in a length gauge. The gauge length is used should be those specified in the table for the appropriate material.

~ The pieces of aggregates from each fraction tested which could not pass through the specified gauge length with its long side are elongated particles and they are collected separately to find the total weight of aggregate retained on the length gauge from each fraction.

~ The total amount of elongated material retained by the length gauge is weighed to an accuracy of at least 0.1 % of the weight of the test sample.

~ The weight of each fraction of aggregate passing and retained on specified sieves sizes are found - \( W_1, W_2, W_3, \ldots \) And the total weight of sample determined \( = W_1 + W_2 + W_3 + \ldots = W\) g. Also the weights of material from each fraction retained on the specified gauge length are found = \( X_1, X_2, X_3 \ldots \) and the total weight retained determined \( = X_1 + X_2 + X_3 + \ldots = X\) gm.

~ The elongation index is the total weight of the material retained on the various length gauges, expressed as a percentage of the total weight of the sample gauged.

\[
\text{Elongation Index} = \frac{\sum (X_1 + X_2 + X_3 + \ldots)}{W} \times 100
\]
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Length Gauge

Elongation Index Test in Progress
**Observation and Calculation:**

<table>
<thead>
<tr>
<th>Weight of aggregates in each fraction retained on length gauge, gm.</th>
<th>Weight of the fraction consisting of atleast 200 pieces in gm.</th>
<th>LENGTH GAUGE (1.8 TIMES THE MEAN SIEVE) mm</th>
<th>SIZE OF AGGREGATE</th>
<th>PASSING THROUGH I.S. SIEVE mm</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>50</td>
<td></td>
<td>63</td>
</tr>
<tr>
<td></td>
<td></td>
<td>40</td>
<td></td>
<td>50</td>
</tr>
<tr>
<td>81.00</td>
<td></td>
<td>25</td>
<td></td>
<td>40</td>
</tr>
<tr>
<td></td>
<td></td>
<td>25</td>
<td></td>
<td>31.5</td>
</tr>
<tr>
<td></td>
<td></td>
<td>20</td>
<td></td>
<td>25</td>
</tr>
<tr>
<td>40.50</td>
<td></td>
<td>16</td>
<td></td>
<td>20</td>
</tr>
<tr>
<td>32.40</td>
<td></td>
<td>12.5</td>
<td></td>
<td>16</td>
</tr>
<tr>
<td>25.60</td>
<td></td>
<td>10.0</td>
<td></td>
<td>12.5</td>
</tr>
<tr>
<td>20.20</td>
<td></td>
<td>6.3</td>
<td></td>
<td>10</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Result:** The elongation index of a given sample of aggregate is ________________ %. 
SHAPE TEST (Angularity Number)

**Aim:** To determine the Angularity Number of the given aggregate sample.

**Apparatus:**
1. The apparatus consists of a metal cylinder closed at one end and of about 3 liter capacity. The diameter and height of this being approximately equal i.e., about 15.64cms diameter and 15.64cms height.
2. A metal tamping rod of circular cross section 1.6cms in diameter and 60cms in length rounded at one end.
3. I.S. sieves of sizes 20, 16, 5, 10, 6.3 and 4.75mm and balance of capacity 10kg to weigh upto 0.1gm.

**Procedure:**
~ Metal cylinder is calibrated by determining the weight of water at 27°C required to fill it, so that no meniscers is present above the rim of the container.
~ The sample of single size aggregate retained between the specified pair of sieves is dried in an oven at a temperature 100°C to 110°C for 24 hours and cooled prior to testing.
~ The aggregates are placed in the cylinder and subjected to 100 blows of the tamping rod at a rate of about 2 blows per second. Each blow is applied by holding the rod vertically with its rounded end 5cms above the surface of the aggregates and releasing it so that it falls vertically and no force is applied to the rod.
~ The process of filling and tamping is repeated exactly as described above with a second and third layer of aggregate.
~ After the third layer is tamped, the cylinder is filled to over flowing and the aggregates are struck off level with the top using a tamping rod as a straight edge.
~ The aggregate with cylinder is then weighed accurately.
~ All the above steps are repeated on another sample and averages of two are represented.
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The angularity number is calculated from the formula,

\[
\text{Angularity Number} = 67 - \frac{100W}{CG}
\]

\(W\) = Mean weight of aggregates in the cylinder, gm.

\(C\) = Weight of water required in the cylinder, gm.

\(G\) = Specific gravity of aggregate.

**Observation and Calculation:**

<table>
<thead>
<tr>
<th>Average</th>
<th>Trail 2</th>
<th>Trail 5</th>
<th>Details of Sample</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
<td>Weight of aggregate filling the cylinder to the nearest five grams</td>
</tr>
</tbody>
</table>

**Result:** The angularity number of given aggregate sample = _______________________

**Viva Voce:**

1. Explain what is meant by flaky and elongated particles?
2. Explain Angularity Number. How is it found?
3. What do you understand by the term Combined Index?
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Reference:

2. Indian Standard Specifications for Coarse and Fine Aggregate from Natural Sources for Concrete, IS: 383 Indian Standards Institution.
Test No.5

“Unit Weight and Voids in Aggregate in its compacted or loose condition”

(ASTM C 29 – 89)

Scope: This test method covers the determination of unit weight in a compacted or loose condition and calculation of voids in fine and coarse aggregates. This test method is applicable to aggregates not exceeding (100mm) in N.M.S.

Materials:
Sample of, preferably, oven dry fine aggregate and an other of oven-dry coarse aggregate.

Apparatus:
1. A balance accurate to 0.5gm.
2. Measure: A cylindrical metal measure preferably provided with handles. Its capacity shall conform to the limits below:

<table>
<thead>
<tr>
<th>N.M.S (mm)</th>
<th>Capacity of measure (m³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>12.5</td>
<td>0.0028</td>
</tr>
<tr>
<td>25</td>
<td>0.0093</td>
</tr>
<tr>
<td>37.5</td>
<td>0.014</td>
</tr>
<tr>
<td>100</td>
<td>0.028</td>
</tr>
</tbody>
</table>

Note: - The indicated size measure may be used to test aggregate of N.M.S equal to or smaller than that listed.

3. Tamping Rod (A round, straight steel rod (16mm) in diameter and approximately 600mm in length with a rounded to a hemispherical tip.
4. Containers and shovel or scoop.
**Procedure:**

**A- Calibration of the measure:**

1. Fill the measure with water at room temperature and cover with a piece of plate glass in such away as to eliminate bubbles and excess water.
2. Determine the weight of the water in the measure.
3. Measure the temperature of water and determine its density from table below:-

<table>
<thead>
<tr>
<th>Temperature (°C)</th>
<th>Density (kg/m³)</th>
</tr>
</thead>
<tbody>
<tr>
<td>15.6</td>
<td>999.01</td>
</tr>
<tr>
<td>18.3</td>
<td>998.54</td>
</tr>
<tr>
<td>21.1</td>
<td>997.97</td>
</tr>
<tr>
<td>23</td>
<td>997.54</td>
</tr>
<tr>
<td>23.9</td>
<td>997.32</td>
</tr>
<tr>
<td>26.7</td>
<td>996.59</td>
</tr>
<tr>
<td>29.4</td>
<td>995.83</td>
</tr>
</tbody>
</table>

**Note:** Use interpolating if necessary.

4. Calculate the volume, V of the measure by dividing the weight of water required to fill the measure by its density.

**B- Procedure of the test:-**

1. Weigh the cylinder (empty).
2. Fill the cylinder to overflowing by means of a shovel or scoop, discharging the aggregate from a height not to exceed 50mm above the top the cylinder edge. Exercise care to prevent, so far as possible, segregation of the particle sizes of which the sample in composed. Level the surface of the aggregate with the fingers or straight edge in such way that any slight projections of the larger pieces of the coarse aggregate approximately balance the larger voids in the surface below the top of the cylinder.
3. Determine the weight of the measure plus its contents, and calculate the weight of the aggregate by subtracting the empty weight of the cylinder.
4. Empty the cylinder and refill it again to one third of its height and rod the layer of aggregate with (25) strokes of the tamping rod evenly distributed over the surface. Fill the cylinder two-thirds full and again level and rod as previous. Finally, of the cylinder to overflowing and rod again in the manner previously mentioned. Level the surface of the aggregate with the fingers or a straight edge in such away as that mentioned in (step 3).

5. In Roding the first layer, do not allow the rod to strike the bottom of the measure forcibly. In Roding the second layer and third layer, use only enough force to cause the tamping rod to penetrate the previous layer of aggregate.

6. Determine the weight of the measure plus its contents and calculate the wt. Of aggregate.

7. Repeat the same procedure for the fine aggregate sample.

**Calculations:**

**1-Unit weight:** calculate the unit weight for the rodding or shoveling procedure

\[ M = \frac{(G-T)}{V} \]

Where :
- \( M \) = unit weight of the aggregate (kg/m\(^3\))
- \( G \) = Weight of the aggregate plus the cylinder (kg)
- \( T \) = Weight of the empty cylinder (kg)
- \( V \) = Volume of the cylinder (m\(^3\))

Note: The unit weight determined by this test method is for aggregate in an oven-dry condition.

**2-Void content:** Calculate the void content in the aggregate using the unit weight determined by either the rodding or shoveling procedure as follows:

\[ \text{%void} = \frac{\left(\frac{S}{W}\right) - (M) \times 100}{\left(\frac{S}{W}\right)} \]

Where
- \( S \) = bulk specific gravity (from tests 2+3)
- \( W \) = density of water (1000kg/m\(^3\))
3. Put your results in a table like that shown below.

<table>
<thead>
<tr>
<th></th>
<th>Coarse Aggregate</th>
<th>Fine Aggregate</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>Loose</td>
<td>Compacted</td>
</tr>
<tr>
<td>Unit weight kg/m$^3$</td>
<td></td>
<td></td>
</tr>
<tr>
<td>%Voids</td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

**Note:**
Normal-Weight aggregate density: (1280-1920) kg/m$^3$

Fig. (8) The cylindrical metal measures for the fine and coarse aggregates
Test No.6

“Sieve Analysis of fine and coarse aggregates”

(ASTM C 136-84a)

Scope: This method covers the determination of the particle size distribution of the fine and coarse aggregate by sieving.

Materials:
1. The weight of test sample of fine aggregate shall be, after drying, approximately (500 gm).
2. The weight of test sample of coarse aggregate shall conform with the following:

<table>
<thead>
<tr>
<th>N.M.S (mm)</th>
<th>Minimum Weight (kg)</th>
</tr>
</thead>
<tbody>
<tr>
<td>9.5</td>
<td>1</td>
</tr>
<tr>
<td>12.5</td>
<td>2</td>
</tr>
<tr>
<td>19</td>
<td>5</td>
</tr>
<tr>
<td>25</td>
<td>10</td>
</tr>
<tr>
<td>37.5</td>
<td>15</td>
</tr>
</tbody>
</table>

Apparatus:
1. Balance: For fine aggregate accurate for 0.5gm.
   For coarse aggregate accurate for 0.5gm.
2. Containers to carry the sample.
3. Oven.
4. Mechanical Sieve shaker.
5. Two sets of sieve:-For fine aggregate [No.4, No.8, No.16, No.30, No.50, No.100]
   For coarse aggregate [37.5mm, 19mm, 9.5mm, No.4, No.8]
   In addition to a pan and a cover for each set.

Procedure:
1- Put the sample in the oven at 110°C.
2- Determine the empty weight for each sieve and record.
3- Nest the sieve in order of decreasing size of opening from top to bottom place the sample on the top sieve.
4- Agitate (shake) the sieve by placing the set on the mechanical shaker for 10min.
5- Open the set of sieve carefully so that no loosing of materials is expected.
6- Weigh each sieve with the residue record its weight.
7- Tabulate your data in a suitable shape.
8. Make sure that the summation of the residue weights equals to the original sample weight with a difference not more than 1% of the original weight.
9- The table should contain:

<table>
<thead>
<tr>
<th>No. of sieve</th>
<th>Sieve empty Wt</th>
<th>Sieve +residue Wt</th>
<th>Residue Wt</th>
<th>Residue %</th>
<th>% Cum Residue</th>
<th>% Passing</th>
</tr>
</thead>
</table>

10- Fineness Modulus for fine aggregate can be determined as:
F.M. = \( \frac{\Sigma \text{cumulative residue percentage}}{100} \)

It must be within (2.6 - 3.1) for sand.

**Notes:**

1- The sieves dimensions are:

<table>
<thead>
<tr>
<th>No. of sieve</th>
<th>100</th>
<th>50</th>
<th>30</th>
<th>16</th>
<th>8</th>
<th>3/8&quot;</th>
<th>1/2&quot;</th>
<th>3/4&quot;</th>
<th>1&quot;</th>
<th>1.5&quot;</th>
</tr>
</thead>
<tbody>
<tr>
<td>Size of opening (mm)</td>
<td>0.150</td>
<td>0.3</td>
<td>0.6</td>
<td>1.18</td>
<td>2.36</td>
<td>4.75</td>
<td>9.5</td>
<td>12.5</td>
<td>19</td>
<td>25.4</td>
</tr>
</tbody>
</table>

2- The results must be companied with ASTM Specification [C33-99a]

a- For Fine aggregate:

<table>
<thead>
<tr>
<th>Sieve No.</th>
<th>Sieve size</th>
<th>% Passing</th>
</tr>
</thead>
<tbody>
<tr>
<td>3/4&quot;</td>
<td>1.9mm</td>
<td>100</td>
</tr>
<tr>
<td>No.4</td>
<td>4.75mm</td>
<td>95-100</td>
</tr>
<tr>
<td>No.8</td>
<td>2.36mm</td>
<td>80-100</td>
</tr>
<tr>
<td>No.16</td>
<td>1.18mm</td>
<td>50-85</td>
</tr>
<tr>
<td>No.30</td>
<td>0.600mm</td>
<td>25-60</td>
</tr>
<tr>
<td>No.50</td>
<td>0.3mm</td>
<td>10-30</td>
</tr>
<tr>
<td>No.100</td>
<td>0.15mm</td>
<td>2-10</td>
</tr>
</tbody>
</table>

b- For Coarse aggregate: See table (2).
<table>
<thead>
<tr>
<th>Size Number</th>
<th>Nominal Size (Sieves with Square Openings)</th>
<th>100 mm (4 in.)</th>
<th>90 mm (3/8 in.)</th>
<th>75 mm (3 in.)</th>
<th>63 mm (2 1/2 in.)</th>
<th>50 mm (2 in.)</th>
<th>37.5 mm (1 1/2 in.)</th>
<th>25.0 mm (1 in.)</th>
<th>19.0 mm (3/4 in.)</th>
<th>12.5 mm (1/2 in.)</th>
<th>9.5 mm (3/8 in.)</th>
<th>4.75 mm (No. 4)</th>
<th>2.36 mm (No. 8)</th>
<th>1.18 mm (No. 16)</th>
<th>0.08 mm (No. 50)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>50 to 37.5 mm (2 3/4 to 1 1/4 in.)</td>
<td>100</td>
<td>25 to 60</td>
<td>0 to 15</td>
<td>0 to 5</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>03 to 37.5 mm (2 1/4 to 1 1/2 in.)</td>
<td>0 to 100</td>
<td>35 to 70</td>
<td>0 to 15</td>
<td>0 to 5</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>50 to 25.0 mm (2 to 1 in.)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>357</td>
<td>50 to 4.75 mm (2 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>4</td>
<td>37.5 to 19.0 mm (1 1/4 to 3/4 in.)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>467</td>
<td>37.5 to 19.0 mm (1 1/4 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
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<tr>
<td>5</td>
<td>25.0 to 12.5 mm (1 1/4 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>56</td>
<td>25.0 to 9.5 mm (1 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>57</td>
<td>25.0 to 9.5 mm (1 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>6</td>
<td>19.0 to 9.5 mm (3/4 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>67</td>
<td>19.0 to 9.5 mm (3/4 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>7</td>
<td>12.5 to 9.5 mm (1/2 in. to No. 4)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>8</td>
<td>9.5 to 2.36 mm (3/8 in. to No. 8)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>89</td>
<td>9.5 to 1.18 mm (3/16 in. to No. 16)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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<tr>
<td>9a</td>
<td>4.75 to 1.18 mm (No. 4 to No. 16)</td>
<td>0 to 100</td>
<td>90 to 100</td>
<td>0 to 15</td>
<td>0 to 5</td>
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</tbody>
</table>

* Although size 0 aggregate is defined in Terminology C 125 as a fine aggregate, it is included as a coarse aggregate when it is combined with a size 8 material to create a size 89, which is a coarse aggregate as defined by Terminology C 125.
Fig. (9) The Mechanical Sieve Shaker.
Test No.7

“Materials Finer than 75µm (No. 200) Sieve in Mineral Aggregate by Washing”

(ASTM C117-87)

Scope: This test method covers determination of the amount of materials finer than a 75µm (No.200) sieve in aggregate by washing. Clay particles and other aggregate particles that are dispersed by the wash water, as well as water–soluble materials, will be removed from the aggregate during the test.

Materials:

The mass of the test sample, after drying, shall conform with the following:

<table>
<thead>
<tr>
<th>Nominal Max. Size</th>
<th>Minimum Mass (gm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>4.5mm or smaller</td>
<td>300</td>
</tr>
<tr>
<td>9.5mm</td>
<td>1000</td>
</tr>
<tr>
<td>19mm</td>
<td>2500</td>
</tr>
<tr>
<td>37.5mm or larger</td>
<td>5000</td>
</tr>
</tbody>
</table>

Apparatus:

1- Balance accurate to 0.1g or 0.1% of the test mass, whichever greater.
2- Sieves: 75µm (No.200) sieve + 1.18mm (No.16) sieve.
3- Container.
4- Oven.

Procedure:

1- Dry the test sample to constant mass at a temperature of $110 \pm 5^\circ C$. Determine the mass to the nearest 0.1gm of the test sample.
2- Place the test sample in the container and add sufficient water to cover it. Agitate the sample to result in complete separation of all particles finer than the 75µm (No.200) sieve from the coarser particles, and to bring the fine materials into suspension. Immediately pour the wash water containing the suspended and dissolved solids over the nested sieves, arranged with the coarser sieve on top.
3- Add a second charge of water to the sample in the container, agitate, and decant as before. Repeat this operation until the wash water is clear.
4- Return all materials retained on the nested sieve by flushing to the washed sample. Dry the washed sample to constant mass at a temp. of 110 + 5 °C and determine the mass to the nearest 0.1% of the original mass of the sample.

5- Calculate the amount of materials passing 75µm (No.200) sieve by washing as follows:

\[ A = 100 \times \frac{B - C}{B} \]

Where:
A = percentage of material finer than 75µm sieve by washing.
B = Original dry mass of sample (gm)
C = Dry mass of sample after washing (gm)

**Note:**
According to [C33-99a] ASTM, [A] must be not more than (3%), in fine aggregate for concrete.
Cement Testing
**BLAINE'S AIR PERMEABILITY TEST**

**Theory and Scope:**

The degree of fineness of cement is a measure of the mean size of the grains in the cement. The rate of hydration and hydrolysis and consequent development of strength depends upon the fineness of cement. To have the same rate of hardening in different brands of cement, the fineness has been standardized. The finer cement has quicker action with water and gains early strength though it's ultimate strength remains unaffected. However the shrinkage and cracking of cement will increase with fineness of cement.

**Aim:** To determine the specific surface of cement Pozzo1onas.

**Apparatus:** The Blaine's variable flow air permeability apparatus.

**Procedure:**

Calibration of the Blaine apparatus.

~ Calculate the volume of the compacted bed of cement V by the following formula $V = \frac{(W_A - W_B)}{P}$

Where $W_A$ = mass of the mercury required to fill the permeability cell

$W_B$ = mass of the mercury to fill the portion of the cell not occupied by the bed of cement formed by 2.8 gm of standard cement sample.

$P$ = Density of mercury at the temperature of test.

The masses $W_A$ and $W_B$ are obtained by weighing the mercury in the crucible.

~ Determine the mass of sample W required to produce a bed having porosity of 0.500 ($= e$) as follows

$W = 3.15V \times (1 - e)$
~ Evacuate the air until the fluid moves above the upper line without pulling it over the top of the side outlet close the valve and note the time $T_s$ taken by manometer liquid to fall from $2^{nd}$ mark (from top) to the $3^{rd}$ mark on the manometer when the air allowed to permeate through the compacted bed of standard cement sample. Note the air temperature.

**Specific surface determination:**

~ Weigh an amount of cement sample equal to that determined in step 2, and the calibration.

~ Place the perforated disc in the permeability cell, then add a filter paper, followed by the sample and another filter paper. Compress the specimen with plunger and couple the permeability cell with the manometer.

~ Evacuate the air until the fluid moves above the upper line without pulling it over the top of side tube. Close the valve of manometer and note the time $T$ it takes for the fluid to drop from the $2^{nd}$ mark to the $3^{rd}$ mark on the manometer when the air is allowed to permeate through the compacted bed of cement obtained in step 5, note the air temperature.

~ Calculate the specific surface $S$ in sqcm/gm of the tested cement by using the following formula with the temperature at the calibration and at the time of test are within $\pm 3\%$ of each other.

\[
S = S_s \cdot \frac{T_s}{T}
\]

Where $S_s =$ Specific surface of standard cement used in calibration.

$T_s =$ Measured time in sec required for the fluid to fall the middle interval for standard sample.

$T =$ Measured time In sec required for the fluid to drop over the middle interval.

~ Compare the test values with the specified values of the cement sample used.
Perforated metal disc
with 30 to 40 holes
t mm ~ EQ tally
distributed

MANOMETER

Blaine Air Permeability Apparatus
Observations and Calculations: a)

Calibration data

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Unit</th>
</tr>
</thead>
<tbody>
<tr>
<td>Apparatus identification</td>
<td></td>
</tr>
<tr>
<td>Mass of empty crucible, gm</td>
<td>gm</td>
</tr>
<tr>
<td>Mass of crucible + mercury required to fill the cell, gm</td>
<td>gm</td>
</tr>
<tr>
<td>Mass of mercury required to fill the cell, W gm</td>
<td>gm</td>
</tr>
<tr>
<td>Mass of crucible + mercury required to fill the portion of the cell above the cement bed, gm</td>
<td>gm</td>
</tr>
<tr>
<td>Mass of mercury required to fill the portion of the cell above the cement bed, WBgm</td>
<td>gm</td>
</tr>
<tr>
<td>Bulk volume of compacted bed of cement, V cm³</td>
<td>cm³</td>
</tr>
<tr>
<td>Mass of sample, W gm</td>
<td>gm</td>
</tr>
<tr>
<td>Average time taken by manometer liquid to fall from 2\textsuperscript{nd} to 3\textsuperscript{rd} line, Ts sec</td>
<td>sec</td>
</tr>
<tr>
<td>Air temperature in °C</td>
<td>°C</td>
</tr>
<tr>
<td>Specific surface of the standard cement, Ss cm²/gm</td>
<td>cm²/gm</td>
</tr>
</tbody>
</table>

b) Fineness determination

<table>
<thead>
<tr>
<th>Identification</th>
<th>gm</th>
</tr>
</thead>
<tbody>
<tr>
<td>Sample W in gm</td>
<td>gm</td>
</tr>
<tr>
<td>Air temperature, °C</td>
<td>°C</td>
</tr>
<tr>
<td>Time for liquid to fall through the middle, sec</td>
<td>sec</td>
</tr>
<tr>
<td>Average time, T sec</td>
<td>sec</td>
</tr>
<tr>
<td>Specific surface, cm²/gm</td>
<td>cm²/gm</td>
</tr>
</tbody>
</table>
Result: The fineness of the given cement sample = ___________________

Viva voce:
1. What does the fineness of the cement indicate?
2. The specific surface by air permeability methods for different cements are:-
   b) Ordinary cements
   c) Rapid hardening cement
   Low heat cement
3. Does it give any idea of the particle sizes present in the sample?

References:
Test No.8

“Fineness of Hydraulic Cement by No.100 or No. 200 Sieve”

(ASTM C 184-83)

Scope: This test method covers determination of the finesses of hydraulic cement by means of the 150 µm (No.100) and 75µm (No.200) sieves.

Apparatus:
1. Sieve: Standard 150 µm (No.100) or 75µm (No.200) sieves.
2. Balance and weights.
3. Brush: a bristle brush will be required for use in cleaning the 150 µm or 75µm sieve.
4. A pan and a cover for the sieve.

Procedure:
1. Place 50-gm sample of the cement on the clean, dry (No.100) or (No.200) sieve with the pan attached.
2. While holding the sieve and uncovered pan in both hands, sieve with a gentle wrist motion until most of the fine material has passed through and the residue looks fairly clean. 13 or 4 minutes.
3. Place the cover on the sieve and remove the pan.
4. With the sieve and cover held firmly in one hand, gently tap the side of the sieve with the handle of the brush used for cleaning the sieve.
5. Empty the pan and wipe it out with a cloth, replace the sieve in the pan and carefully remove the cover.
6. Continue sieving without the cover for 5 to 10 min. Or until not more than (0.05gm) of the material passes through in 1 minutes of continuous sieving.
7. Carefully open the set and transfer the residue on the sieve to a white clean paper, and record the weight.
8. Calculate the percentage residue as:

   \[
   \% \text{ residue} = \frac{\text{wt. of residue} \times 100}{50}
   \]

9. Specifications requires that %retained on sieve (No.200) Shall not exceed 22%. and on sieve (No.100) not more than 10%.
Test No.9

“Normal Consistency of Hydraulic Cement”

ASTM (C 187-86)

Scope: This test method covers the determination of the normal consistency of hydraulic cement. That is by determining the amount of water required to prepare cement pastes for Initial and final time of setting test.

Apparatus:
1. Weight and weighing devices.
2. Glass graduates (200 or 250) ml capacity.
3. Vicat apparatus with the plunger end, 10 mm in diameter.
4. Electrical mixer, trowel and containers.
5. Mixing glass plate 30cm x 30cm.

Procedure:

1- Place the dry paddle and the dry bowl in the mixing position in the mixer.

2- Place all the mixing water in the bowl.

3- Add the cement to the water and allow 30 s for a absorption of the water.

4- Start the mixer at low speed for 30 s

5- Stop for (15 s) and make sure no materials have collected on the sides of the bowl.

6- Start mixing at medium speed for (1 min).

7- Quickly form the cement paste into the approximate shape of a ball with gloved hands.

8- Putting hand at (15cm) distance, throw the cement paste ball from hand to hand six times.

9- Press the ball into the larger end of the conical ring, completely fill the ring with paste.

10- Remove the excess at the larger end by a single movement of the palm of the hand. Place the ring on its larger end on the base of the plate of Vicat apparatus.
11- Slice off the excess paste at the smaller end at the top of the ring by a single sharp-ended trowel and smooth the top. (Take care not to compress the paste).

12- Center the paste under the plunger end which shall be brought in contact with the surface of the paste, and tighten the set-screw.

13- Set the movable indicator to the upper zero mark of the scale or take an initial reading, and release the rod immediately. This must not exceed 30 seconds after completion of mixing.

14- The paste shall be of normal consistency when the rod settles to a point 10±1mm below the original surface in 30 seconds after being released.

15- Make trial paste with varying percentages of water until the normal consistency is obtained. Make each trial with fresh cement.

16- Prepare a table in the form:

<table>
<thead>
<tr>
<th>W/c</th>
<th>Weight of cement (gm)</th>
<th>Water Volume (ml)</th>
<th>Penetration (mm)</th>
</tr>
</thead>
<tbody>
<tr>
<td>24%</td>
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<tr>
<td>26%</td>
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<tr>
<td>28%</td>
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<tr>
<td>30%</td>
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</tbody>
</table>

17. Draw the penetration — w/c curve.
18. From the curve state the w/c% which will give (10mm), that is the percentage for Normal Consistency.

Fig.(10) The Vicat Apparatus.
Test No. 10

“Initial and Final Time of Setting of Cement”
(ASTM C191-82)

Scope: This test covers determination of the time of Setting of cement by means of
the Vicat needle.

Apparatus:
1. Vicat Apparatus with the needle end, 1mm in diameter.
2. Weights and weighing Device.
3. Glass Graduates (200 or 250) ml capacity.
4. A trowel and containers.

Procedure:
1. Weigh (400) gm cement.
2. Prepare amount of water as to that calculated in normal consistency test.
3. Prepare a cement paste following same steps mentioned in the previous test (test
   No. 9). Place in Vicat conical ring like test No. 9. Don't forget to record the
time since the cement is added to the water.
4. Allow the time of setting specimen to remain in the moist cabinet for 30 minutes
   after molding without being disturbed. Determine the Penetration of the 1mm
   needle at this time and every (15) minutes until a penetration of 25mm or less is
   obtained
5. To read the penetration, lower the needle of Vicat Apparatus until it touches the
   surface of the cement paste. Tighten the screw and take an initial reading. Release
   the set screw and allow the needle to settle for 30 seconds, and then take the
   reading to determine the penetration.
6. Note that no penetration shall be made closer than (6mm) from any previous
   penetration and no penetration shall be made closer than (9.5mm) from the inside
   of the mold. Record the results of all penetration, then by drawing a curve
determine the time when a penetration of 25 mm is obtained. This is the initial
   setting time
7. The final setting time is when the needle dose not sinks visible into the paste.
8. Draw a graph for (penetration — time). Show the time which gives penetration of
   (25 mm) this will be the initial setting time.

Note:

According to ASTM C150:

Initial time of setting, not less than 45 min.

Final time of setting, not more than 375 min.
Test No.11

“Density and Specific Gravity of cement”
(ASTM C188-87)

Scope:
This test covers determination of the density of cement and its specific gravity. The density of cement is defined as the mass of a unit volume of the solids.

Apparatus:
1- Le chatelier flask: the standard flask which is circular in cross section with special shape and dimensions
2- Kerosene, free of water.
3- Balance.
4- Holder.
5- Water bath.

Procedure:
1- Fill the flask with Kerosene to a point on the stem between 0 and 1ml mark.
2- Put the flask in the water bath at a constant temperature for a sufficient period of time in order to avoid flask temperature variations greater than 0.2 °C between the initial and final readings.
3- Record the final reading on the flask.
4- Prepare (64) gm of cement weighed to the nearest (0.05) gm and place it in the flask in small increments. Take care to avoid splashing and see that the cement dose not adheres to the inside of the flask above the liquid.
5- After all the cement has been introduced, place the stopper in the flask and roll the flask in an inclined position so as to free the cement from air until no further air bubbles rise to the surface of the liquid.
6- Put the flask in the water bath as in step (2).
7- Take the final reading.

Calculations:
1- The difference between the first and the final readings represents the volume of liquid displaced by the mass of cement used in the test.
2- Calculate the cement density \( \rho \) as:

\[
\rho_{\text{cement}} = \frac{\text{Mass of cement}}{\text{Volume}}
\]

Specific Gravity = \( \rho_{\text{cement}} / \rho_{\text{water}} \)
Fig.(11) Le Chatelire flask.
Test No. 1

“Compressive Strength of Hydraulic Cement Mortars"

"Using 50 mm Cube Specimens”

( ASTM C109-88 )

Scope
This test method covers determination of the compressive strength of cement mortars, using 2 in (50 mm) cube specimens.

Apparatus
1- Weights and weighing device.
2- Glass Graduate.
3- Specimens molds: three cubes of (50mm) side.
4- Mixer (electrically driven mechanical mixer of the type equipped with paddle and mixing bowl).
5- Testing machine.
6- Tamper and trowel.

Materials:
Graded standard sand should be used (C778) with cement in the proportion 1 Cement : 2.75 Sand by weight. Use water – cement ratio of 0.485 for all Portland cements and 0.460 for all air-entraining Portland cements.

Note: For other than Portland and air-entraining Portland cements, do flow table test, to determine the amount of mixing water.

Procedure:
A. Preparation of Mortar :-

1. Weigh (300)gm of cement and Prepare the corresponding weights of standard sand and water.

2. Place the dry paddle and the dry bowl in the mixing position in the mixer. Then introduce the materials for a batch into the bowl and mix in the following manner:
   i- Place all the mixing water in the bowl.
   ii- Add the cement to the water, then start the mixer and mix at the low speed (140 ± 5 r/min) for (30 s).
   iii- Add the entire quantity of sand slowly over a (30 s) period, while mixing at slow speed.
iv- Stop the mixer, change to medium speed (285 ±10 r/min) and mix for 30 s.
v- Stop the mixer and let the mortar stand for 1.5 min. During the first (15 s) of this interval, quickly scrape down into the batch any mortar that may have collected on the side of the bowl.

vi- Finish by mixing for (1 min) at medium speed.

**B-Molding test specimens:**
i- Thinly cover the interior faces of the specimen molds with oil.
ii- Start molding the specimens within a total time of not more than 2.5 min after completion of mixing.
iii- Place a layer of mortar about 25 mm (half the depth of the mold) in all the cube specimens.
iv- Tamp the mortar in each cube 32 times (4x8), about 4 rounds, each round to be at right angles to the other.

![Tamping Diagram]

The tamping pressure shall be just sufficient to insure uniform filling of the molds.
v- The 4 rounds of tamping shall be completed in one cube before going to the next.
vi- When the tamping of the first layer in all cubes is completed, fill the molds with the remaining mortar and tamp as specified for the first layer.
vii- Cut off the mortar to a plane surface with a straight edge.
viii- Keep the molds in a moist room for 20-24 hours then open them and keep the specimens in a water basin for a week.

**C-Testing specimens:**
1- After 7 days (± 3 hours), take the specimens out of the basin, dry them with a clean cloth, put them, one after the other, in the testing machine.
2- The cubes must be put on one side, using extra steel plates up and down the specimen.
3- Start loading in a speed of 1.4 kN/sec or (350 kg/cm²) in a minute.
4- When failure, record load and the compressive strength.

**Calculations:**

1- Table the results:

<table>
<thead>
<tr>
<th>Cube No.</th>
<th>Load(kN)</th>
<th>Compressive strength( MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td></td>
</tr>
</tbody>
</table>

2- Compare with [ASTM C150-89]: \( \sigma_c \geq 19.3 \text{ MPa} \) [For type I cement] age 7 days
Fig. (1) The mixer to be used to mix the mortar.

Fig. (2) The specimens molds.
Test No. 2

Tensile Strength of Cement Mortar
(ASTM C 190-85)

**Scope:**
This test method covers the determination of the tensile strength of cement mortars employing the Briquet specimens.

**Apparatus:**
1- Weights and weighing device.
2- Tools and containers for mixing.
3- Briquet molds.
4- Water basin.
5- Testing Machine.

**Procedure:-**

1- The proportions of materials for the standard mortar shall be 1 part of cement to 3 parts standard sand by weight. For making 3 briquets, prepare 300 gm of cement with 3x300 = 900 gm of standard sand. The percentage of water used in the standard mortar shall depend upon the percentage of water required to produce a neat cement paste of normal consistency from the same sample of cement as in table (1).

<table>
<thead>
<tr>
<th>Water for neat cement paste of Normal Consistency %</th>
<th>Water for Mortar of 1 part Cement to 3 parts standard Sand %</th>
</tr>
</thead>
<tbody>
<tr>
<td>9</td>
<td>15</td>
</tr>
<tr>
<td>9.2</td>
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<td>11</td>
<td>27</td>
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<tr>
<td>11.2</td>
<td>28</td>
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<tr>
<td>11.3</td>
<td>29</td>
</tr>
<tr>
<td>11.5</td>
<td>30</td>
</tr>
</tbody>
</table>
Note:
The values being in percentage of the combined dry weights of the cement and standard sand.

2- Mix dry cement with dry sand and make a crater in the middle, then pour water in the crater, and turn the material on the outer edge into the crater within 30 seconds by the aid of a trowel.
3- After an additional interval of 30 seconds for the absorption of the water, mix thoroughly for 1.5 minutes.
4- Prepare Briquet molds, clean and thinly covered with a film of mineral oil.
5- Fill the molds heaping full without compacting, then press the mortar in, firmly with the thumbs, applying the force 12 times to each Briquet at points to include the entire surface.
6- Heap the mortar above the mold and smooth it off with a trowel.
7- Cover the mold with a plane glass and turn over the mold and plates. Remove the top plate and repeat the operation of heaping, thumbing and smoothing off.
8- Keep all test specimens in moist room for 24 hours.
9- Open molds and immerse the specimens in water in the storage tank. Keep them in water for a week.
10- Take specimens out of water, dry with clean cloth then fix them in the testing machine (one after the other).
11- Record the load causing failure and the cross-sectional area at the fracture point.

Calculation:-

\[
\text{Tensile strength } \sigma_t = \frac{\text{Load causing failure (P)}}{\text{Area at the fracture (A)}}
\]

Note:
According to [ ASTM C 150-58]
\[
\sigma_t \geq 1896 \text{ kPa} \text{ [ For type 1 cement → 1 days in moist air +6 days in water ]}
\]
Fig. (3) The testing machine for cement mortar specimens in tension.

Fig. (4) The briquete molds.
Test No. 3

"Making and Curing Concrete Test Specimens in the Laboratory"
[ASTM C192-88]

Scope:
This practice cover procedures for making and curing test specimens of concrete in the laboratory under accurate control of materials and test conditions using concrete that can be consolidated by rodding or vibration.

Procedure for mixing Concrete:

General: -
1- Mix concrete in a suitable mixer or by hand in batches of such size as to leave about 10% excess after molding the test specimens.
2- Hand-mixing procedures are not applicable to air-entrained concrete or concrete with no measurable slump.
3- It is Important not to vary the mixing sequence and procedure from batch to batch unless the effect of such variation is under study.

Machine Mixing:
1- Put the coarse aggregate in the mixer, add some of the mixing water and the solution of admixture, when required, [add with water].
2- Start the mixer, then add the fine aggregate, cement and water with the mixer running. If it is impractical to add the fine aggregate, cement and water with the mixer is running, these components may be added to the stopped mixer after permitting it to turn a few revolutions following charging with coarse aggregate and some of the water.
3- Mix the concrete, after all integrates are in the mixer, for 3 minutes followed by 3 minutes rest, following by 2-minutes final mixing.

Hand Mixing:
1- In a watertight clean, damp metal pan, mix the cement, insoluble admixture, if used, and the fine aggregate without addition of water until they are thoroughly blended.
2- Add the coarse aggregate and mix the entire batch without addition of water until the coarse aggregate is uniformly distributed throughout the batch.
3- Add water, and the admixture solution if used, and mix the mass until the concrete is homogenous in appearance and of the desired consistency.
Making Specimens:

1- Place of Molding:
   i- Mold specimens as near as practicable to the place where they are to be stored during the first 24 hours.
   ii- Place molds on a rigid surface free from vibration and other disturbances
   iii- If it is not practicable to mold the specimens where they will be stored, move them to the place of storage immediately after being struck off.

2- Placing:
   i- Place the concrete in the molds using a scoop, blunted trowel, or shovel. Select each scoopful, trowelful, or shovelful of concrete from the mixing pan to ensure that it is representative of the batch.
   ii- It may be necessary to remix the concrete in the mixing pan with a shovel to prevent segregation during the molding of specimens.
   iii- Move the scoop or trowel around the top edge of the mold as the concrete is discharged in order to ensure symmetrical distribution of the concrete and for minimize segregation of coarse aggregate within the mold.
   iv- Further distribute the concrete by use of a tamping rod prior to the start of consolidation.

3- Number of layers:
   Make specimens, in layer as indicated by the test for which they are prepared or as [ASTM C 192-table1].

4- Methods of consolidation:
   Preparation of satisfactory specimens requires different methods of consolidation. The methods of consolidation are:
   i- Rodding.
   ii- Internal vibration.
   iii- External vibration.

Hints:
   - Rod concretes with slump greater than 75mm.
   - Rod or vibrate concretes with slump of (25-75mm).
   - Consolidate by vibration concrete with slump of less than 25mm.
   - Do not use internal vibration for cylinders of 100mm diameter or less and beams or prisms of 100mm breadth or depth or less.

i- Rodding:
   Place the concrete in the mold in the required number of layers of approximately equal volume. Rod each layer with the rounded end of the rod using the number of strokes and size of rod specified in table (2) ASTM C 192-88.
   Rod the bottom layer throughout its depth. Distribute the strokes uniformly over the cross-section of the mold and for each upper layer allow the rod to penetrate about 12mm into the underlying layer when the depth of the layer is less than 100mm and about (25mm) when the depth is (100mm) or more.
   After each layer is rodded, tap the outside of the mold lightly 10-15 times with the mallet to close any holes left by rodding.
ii) Vibration

The duration of vibration required will depend upon the workability of the concrete and the effectiveness of the vibrator. Continue vibration only long enough to achieve proper consolidation of the concrete. Fill the molds and vibrate in the required number of approximately equal layers. Place all the concrete for each layer in the mold before starting vibration of that layer. Add the final layer, so as to avoid over filling by more than (6 mm). Then finish the surface.

5- Finishing:
After consolidation, strike off the surface of the concrete and float or trowel it with a wood or magnesium float.

6- Curing:
1- Covering after finishing: To prevent evaporation of water from the unhardened concrete cover the specimens immediately after finishing, preferably with a non-absorptive, non reactive plate.
2- Removal from molds: Remove the specimens from the molds after 24 ± 8 hours.
3- Curing Environment: Unless otherwise specified, all specimens shall be moist cured at 23 ± 1.7 °C from the time of molding until the moment of test.
Concrete Testing
Test No. 4:

“The Slump of hydraulic Cement Concrete”
[ASTM C143-89a]

Scope:
This test method is used to determine the slump of freshly mixed concrete, which is an approximate measure of consistency. The test may be done in the laboratory and in field.

Apparatus:
1- Weights and weighing device.
2- Tools and containers for mixing, or concrete mixer.
3- Tamper (16 mm in diameter and 600 mm length)
4- Ruler
5- Slump cone which has the shape of a frustum of a cone with the following dimensions:
   Base diameter 20 cm
   Top diameter 10 cm
   Height 30 cm
   Materials thickness at least 1.6 mm

Procedure:
1- Prepare a clean, wide, flat mixing pan.
2- Place the dampened slump cone on one side of the pan. It shall be held firmly in place during filling by the operator standing on the two foot pieces.
3- Place the newly mixed concrete (prepared as in test No. 3) in three layers, each approximately one third the volume of the mold.
4- In placing each scoopful of concrete, move the scoop around the top edge of the mold as the concrete slides from it, in order to ensure symmetrical distribution of concrete within the mold.
5- Rod each layer with 25 strokes of the tamper, distribute the strokes in a uniform manner over the cross section of the mold, each stroke just penetrating into the underlying layer.
6- For the bottom layer this will necessitate inclining the rod slightly and making approximately half of the strokes spirally toward the center.
   Rod the bottom layer throughout its depth.
7- In filling and rodding the top layer, heap the concrete above the mold before rodding is started.
8- After rodding the top layer, strike off the surface of the concrete with a trowel, leaving the mold exactly filled.
9- While filling and rodding, be sure that the mold is firmly fixed by feet and can’t move.
10- Clean the surface of the base outside the cone of any excess concrete. Then immediately remove the mold from the concrete by raising it slowly in a vertical direction.
11-Measure the slump immediately by determining the difference between the height of the mold and the height of the vertical axis (not the maximum height) of the specimen.

12- Clean the mold and the container thoroughly immediately after using.

13- If the pile topples [when raising the mold out of concrete] sideways, it indicates that the materials have not been uniformly distributed in the mold and the test should be remade.

Fig. (8) Measuring the slump.

Fig. (9) Different possible slump test results.
Test No. 5

“Compacting Factor Test”
BS 1881: Part 103: 1993

Four methods of determining the workability of fresh concrete are given in Part 102 to 105 of BS 1881, as follows:

<table>
<thead>
<tr>
<th>Workability</th>
<th>Method</th>
</tr>
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<tbody>
<tr>
<td>Very low</td>
<td>Vebe time</td>
</tr>
<tr>
<td>Low</td>
<td>Vebe time, compacting factor</td>
</tr>
<tr>
<td>Medium</td>
<td>Compacting factor, Slump</td>
</tr>
<tr>
<td>High</td>
<td>Compacting factor, Slump, Flow</td>
</tr>
<tr>
<td>Very high</td>
<td>Flow</td>
</tr>
</tbody>
</table>

Scope
This test describes the method for determining the compacting factor of concrete of low, medium and high workability. The method applies to plain and air-entrained concrete, made with lightweight, normal weight or heavy aggregates having a nominal maximum size of 40 mm or less but not to aerated concrete or no-fines concrete.
The method is suitable for concretes having compacting factor in the range 0.7 to 0.98

Apparatus:
1- The compacting factor apparatus, which consists of a holder fixing two conical hoppers and a cylinder at the base.
2- Tools and containers for carrying and mixing the materials.
3- Balance.

Procedure:
1- Prepare a concrete mix following steps mentioned in test (No3). Use 8 kg of cement to cast 2 cubes and 2 cylinders.
2- Damp the two, hoppers and record the empty weight of the cylinder.
3- First, close the bases of the two hoppers.
4- Fill the upper hopper with the freshly mixed concrete (fill freely without compacting), then open the base of this upper hopper to allow concrete to fall under the effect of its weight to the lower hopper. This hopper is smaller than the upper one, thus it will be filled to overflowing.
5- Then open the base of the second hopper to allow concrete (also only under the effect of its weight) to fall into the cylinder. Excess concrete is cut by two floats slide across the top of the mold.
6- Certain mixes have a tendency to stick in one or both of the hoppers. If this occurs, help the concrete through by pushing the tamping rod gently into the concrete from the top until the lower end emerges from the bottom of the hopper. If this does not dislodge the concrete, raise the rod and repeat the process until the concrete falls through the hopper. Count the number of times the concrete is rodded as this provides a guide to the cohesiveness of the concrete.
7- Level the surface of the cylinder and clean the sides of the cylinder.
   Within 150 s of placing, weigh the cylinder with concrete inside. Record the 
   weight.
8- The difference between the weight of the concrete with the cylinder and empty 
   cylinder will be the weight of partially compacted concrete \([W_1]\).
9- Now empty the cylinder, clean it and cover the inside surface by a thin layer of 
   mineral oil.
10- Fill the cylinder with concrete in six layers (BS) rodding each layer by (25) 
    strokes equally distributed on the surface. Level the surface and clean sides.
11- Weigh the cylinder with its contents and record.
12- The difference between the weight of the compacted concrete with the cylinder 
    and the empty cylinder will be the weight of completely compacted concrete \([W_2]\).

**Calculations:**

The compacting factor \((C.F) = \frac{W_1}{W_2} = \frac{\text{The weight of partially compacted concrete}}{\text{The weight of completely compacted concrete}}\)

**Note:** Typical range is \([0.70 \text{ to } 0.98]\)
Test No. 6

“Flow Table Test for Fresh Concrete”
BS1881: Part 105:1984

Scope:
It specifies the method for determination of the flow of concrete of high to very high workability. The method applies to plain and air-entrained concrete, having a flow diameter of 500mm to 650mm when tested, made with light weight, normal weight or heavy aggregates having a nominal maximum size of 20mm or less. It does not apply to aerated concrete or no fines concrete.

Apparatus:
1- The table, which consists essentially of a board covered by a steel plate with a total mass of 16 kg. This board is hinged along one side to a base board, each board being a 700 mm square. The upper board can be lifted up to a stop so that the free edge rises 40mm. Appropriate marking indicate the location of the concrete to be deposited on the table.
2- A frustum of a cone, 200mm high with a bottom diameter of 200 mm and a top diameter of 130 mm
3- A tamping bar, made of a suitable hardwood, having a square section of side 40±1 mm and at least 200mm long.
4- Weights and weighing device.
5- Tools and containers for mixing.
6- Rule of min length 700mm.

Procedure:
1- Prepare a concrete mix as in test No.3, using mix proportions of 1:2:3 and w/c=65%
2- Moist the table top and the frustum of the cone.
3- Try lifting and dropping the table then, keep the table horizontal.
4- Hold the mold firmly in place and fill in two layers, each approximately one half the volume of the mold. Rod each layer with 10 strokes with the wooden tamper.
5- Before lifting the mould, excess concrete is removed, the surrounding table top is cleaned.
6- After an interval of 30 seconds, the mould is vertically, slowly removed within 3-6 seconds.
7- The table top is lifted slowly and allowed to drop, avoiding a significant force against the stop, 15 times, each cycle taking not less than 3.5 and not more than 5 sec.
8- In consequence, the concrete spreads and the maximum spread parallel to the two edges of the table is measured.
9- The average of these two values, given to the nearest mm, represents the flow.
10- A value of 400 mm indicates a medium workability, and 500 mm a high workability.
**Figure 11. Typical flow table**

**Figure 12. Concrete mould**

**Figure 13. Tamping bar**
(a) General view of the flow table

(b) Measurement of the flow diameter

Figure  Typical concrete spread

(a) Good quality flowing concrete showing no segregation at the perimeter of the sample

(b) Lack of cohesion in the concrete has resulted in grout segregation round the perimeter of the sample

Figure  Examples of good quality and segregated concrete mixes
Test No. 7

“The Compressive Strength of Cubic Concrete Specimens”
BS 1881: Part 116: 1983

Scope:
The test method covers determination of compressive strength of cubic concrete specimens. It consists of applying a compressive axial load to molded cubes at a rate which is within a prescribed range until failure occurs. The compressive strength is calculated by dividing the maximum load attained during the test by the cross-sectional area of the specimen.

Apparatus:
1- Weights and weighing device.
2- Tools and containers for mixing.
3- Tamper (square in cross section)
4- Testing machine.
5- Three cubes (150 mm side)

Procedure:
1- Prepare a concrete mix as mentioned in (test No. 3 ) with the proportions suggested such as: 1: 2: 3 with w/c = 55% by mechanical mixer.
2- Prepare three testing cubes; make sure that they are clean and greased or oiled thinly.
3- Metal molds should be sealed to their base plates to prevent loss of water.
4- Fill the cubes in three layers, tamping each layer with (35) strokes using a tamper, square in cross-section with 2.54 cm side and 38.1 cm length, weighing 1.818 kg.
5- While filling the molds, occasionally stir and scrape together the concrete remaining in the mixer to keep the materials from separating.
6- Fill the molds completely, smooth off the tops evenly, and clean up any concrete outside the cubes.
7- Mark the specimens by a slip of paper on which is written the date and the Specimen identification. Leave the specimens in the curing room for 24 hours.
8- After that open the molds and immerse the concrete cubes in a water basin for 7 days.
9- Before testing, ensure that all testing machine bearing surfaces are wiped clean.
10- Carefully center the cube on the lower platen and ensure that the load will be applied to two opposite cast faces of the cube.
11- Without shock, apply and increase the load continuously at a nominal rate within the range of ( 0.2 N/mm².s to 0.4 N/mm².s ) until no greater load can be sustained. On manually controlled machines, as failure is approached, the loading rate will decrease, at this stage operate the controls to maintain, as far as possible, the specified loading rate. Record the maximum load applied to each cube.

Note:
When the cubes are surface dry, or have not been cured in water, immerse them in water, for a minimum of 5 minutes, before testing. They must be tested while they are still wet.
**Type of failure**

Record any unusual feature in the type of failure. Refer to fig. ( ) for examples of satisfactory failure and to fig. ( ) for examples of some unsatisfactory failures.

**Note:** Unsatisfactory failures are usually caused by insufficient attention to the details of making and testing specimens, such as bad molds, bad made specimens or misplacement of cubes in the testing machine or machine fault.

**Calculations**

Calculate the cross-sectional area of the cube face from the checked nominal dimensions. Calculate the compressive strength of each cube by dividing the maximum load by the cross-sectional area. Calculate the average for the three cubes.

![Figure 1. Satisfactory failures](image)

**Fig. (17) Unsatisfactory Failure.**
Fig.(18) The compression machine.
Test No. 8

“Compressive Strength of Cylindrical Concrete Specimens”
( ASTM C 39-86 )

**Scope:**
The test method covers the determination of compressive strength of cylindrical concrete specimens, such as molded cylinders and drilled cores. It is limited to concrete having a unit weight > 800 kg/m³.

**Apparatus:**
1- Weights and weighing device.
2- Tools and containers and pans for mixing, or mixer.
3- A tamper (circular in cross-section) (16 mm in diameter and 600 mm in length).
4- Testing machine.
5- Three cylinders (150mm in diameter and 300mm in height).

**Procedure:**
1- Follow the same steps as in .(test No. 3) in order to prepare a fresh concrete mix.
2- The cylinder also must be clean, lightly oiled, well fixed with the base.
3- Filling the specimens will be also in three layers, roding each layer by (25) strokes using the circular section rod.
4- All other steps are the same as in test No. 6.
5- The test specimens must be tested in the moist condition with a rate of loading (0.14-0.34) MPa.

**Calculation:**
1- Calculate the compressive strength of the specimen by dividing the maximum load carried by the specimen during the test by the average cross-section area .
2- If the specimen length to diameter ratio is less than(1.8), correct the result obtained by multiplying the appropriate correction factor shown in following table:

<table>
<thead>
<tr>
<th>L/D</th>
<th>1.75</th>
<th>1.5</th>
<th>1.25</th>
<th>1</th>
</tr>
</thead>
<tbody>
<tr>
<td>Factor</td>
<td>0.98</td>
<td>0.96</td>
<td>0.93</td>
<td>0.87</td>
</tr>
</tbody>
</table>

**Note:**
Factor are applicable for normal concrete strengths (from13.8-14.4) MPa.
Test No.9

“Splitting Tensile Strength of Cylindrical Concrete Specimens”

(ASTM C496-86)

**Scope:**
This method covers the determination of the splitting tensile strength of cylindrical concrete specimens.

**Apparatus:**
1. Weights and weighing device.
2. Tools, containers and pans for carrying materials & mixing.
3. A circular cross-sectional rod (φ16mm & 600mm length).
5. Three cylinders (φ150mm & 300mm in height).
6. A jig for aligning concrete cylinder and bearing strips.

**Procedure:**
1. Prepare three cylindrical concrete specimens following same steps as test No.3
2. After molding and curing the specimens for seven days in water, they can be tested.
3. Two bearings strips of nominal (1/8 in i.e 3.175mm) thick plywood, free of imperfections, approximately (25mm) wide, and of length equal to or slightly longer than that of the specimen should be provided for each specimen.
4. The bearing strips are placed between the specimen and both upper and lower bearing blocks of the testing machine or between the specimen and the supplemental bars or plates.
5. Draw diametric lines an each end of the specimen using a suitable device that will ensure that they are in the same axial plane. Center one of the plywood strips along the center of the lower bearing block.
6. Place the specimen on the plywood strip and align so that the lines marked on the ends of the specimen are vertical and centered over the plywood strip.
7. Place a second plywood strip lengthwise on the cylinder, centered on the lines marked on the ends of the cylinder.
8. Apply the load continuously and without shock, at a constant rate within the range of 689 to 1380 kPa/min splitting tensile stress until failure of the specimen.
9. Record the maximum applied load indicated by the testing machine at failure. Note the type of failure and appearance of fracture.

**Computations:** Calculate the splitting tensile strength of the specimen as follows:

\[ T = \frac{2P}{\pi L d} \]

Where: 
- \( T \): splitting tensile strength, kPa
- \( P \): maximum applied load indicated by testing machine, kN
- \( L \): Length, m
- \( d \): diameter, m

**Note:** This test is not a true tension test, but it fails in tension and used to indicate the tensile strength of concrete.
Fig.(19) The jig for aligning concrete cylinder and bearing strips

Fig.(20) Fitting the cylinder in the compression machine.
Test No. 10

“Rebound Number of Hardened Concrete”

ASTM C805-85

or

BS 1881:Part202:1986

Scope:
This test is also known as the Schmidt hammer or impact hammer, and is a non-destructive method of testing concrete. The test is based on the principle that the rebound of an elastic mass depends on the hardness of the surface against which the mass impinges.

Apparatus:
1- Rebound hammer.
2- Abrasive stone: consisting of medium-grain texture silicon carbide or equivalent material.

Selection of Test Surface:
Concrete members to be tested shall be at least 100 mm thick and fixed within a structure. Smaller specimens must be rigidly supported. Areas exhibiting honeycombing, scaling, rough texture, or high porosity should be avoided. Concretes should be approximately the same age and moisture condition in order to be compared. Dry concretes give higher rebound numbers than wet concrete, and the surface layer of concrete may be carbonated, yielding higher rebound numbers.

Preparation of test surface:
A test area shall be at least 150 mm in diameter. Heavily textured, soft, or surfaces with loose mortar shall be ground smooth with the abrasive stone. Smooth-formed or toweled surface shall be tested without grinding. Concretes over 6 months old may require grinding to a depth of 5 mm if they are to be compared to younger concretes. Grinding to this depth is not feasible without power equipment.

Procedure:
1- Firmly hold the instrument in a position that allows the plunger to strike perpendicularly to the surface tested. Gradually increase the pressure on the plunger until the hammer impacts.
2- After impact, record the rebound number to two significant figures.
3- Take ten readings from each test area. No two impact tests shall be closer together than 25 mm.

Calculation:
Discard readings differing from the average of 10 readings by more than 5 units and determine the average of the remaining readings. If more than 2 readings differ from the average by 7 units, discard the entire set of readings.
Fig.(21) The calibration of the Schmidt hammer.

Fig.(22) Testing concrete using the Schmidt hammer.
Test No. 11

“Pulse Velocity Through Concrete”

ASTM C598-83

or

BS:1881:Part 203:1986

Scope:
1- This test method covers the determination of the pulse velocity of propagation of compression waves in concrete.
2- The pulse velocity is independent of the dimensions of the body provided reflected waves from the boundaries do not complicate the determination of the arrival time of the directly transmitted pulse.
3- The pulse velocity $V$ is related to the physical properties of a solid by the equation:

$$V^2 = \frac{(K)(E)}{D}$$

Where:
- $K$ = a constant
- $E$ = the modulus of elasticity, and
- $D$ = the density.

The relationship is independent of the frequency of the vibrations.

Apparatus:
1- The apparatus used in this test is called “PUNDIT”. This name is derived from the initial letters of “Portable Ultrasonic Nondestructive Digital Indicating Tester”.
2- Two transducers (54 KHz).
3- Two transducer leads.
4- Reference bar for checking zero.
5- Tin of couplant.

Procedure:
1- Before switching on the PUNDIT, the transducers should be connected to the sockets marked “TRAN” and “REC”. The connection or disconnection of the transmitting transducer should not be made while the instrument switched on. The PUNDIT may be operated from either:
   i) the internal battery,
   ii) an external battery, or
   iii) the A.C. mains supply.

The battery operation is most convenient for field use while the mains operation is generally more suitable for laboratory use.
2- If using the A.C. mains supply, plug the mains cable into the 3 way socket mounted on the rear panel, switch the P.S.S. to MAINS and depress the reset button to switch the PUNDIT ON.

3- Before using the PUNDIT, it should be calibrated using the reference bar. After putting the coupling agent on the transducers faces, the transducers faces are placed and pressed against the reference bar ends, using the “set free button”. The reading of the instrument should be adjusted to read the transit time recorded on the calibration bar.

4- After applying an appropriate coupling agent (such as water, oil, petroleum jelly, grease, or other viscous materials) to the transducer diaphragms, the test surface, or both, to avoid entrapped air between the contact surface of the diaphragms of the transducers and the surface of the concrete. Press the faces of the transducers against the surfaces of the concrete and measure the transit time. Measure the length of the shortest direct path between the centers of the diaphragms.

**Calculation:**

Calculate the pulse velocity as follows:

\[ V = \frac{L}{T} \]

Where:

- \( V \) = pulse velocity, m/s
- \( L \) = distance between transducers, m
- \( T \) = effective transmit time, s
Test No. 12

“Trial method of proportioning for concrete mixes”

Scope:  
This is one of the widely used methods for designing a concrete mix. The method requires that samples of the cement, fine aggregate and coarse aggregate be available and that the relation between water-cement ratio and strength be known or assumed.

Apparatus:  
1- Weights and weighing device.  
2- Tools and containers for mixing.  
3- Slump cone and tamper.

Procedure:  
1- Assuming that a concrete mix is to be designed to be used in some part of a building, say a column.  
2- Assuming that the compressive strength required is 280kg/cm². Referring to table (1) the corresponding w/c ratio is taken to be (0.534) on the assumption that the concrete is without entrained air.  
3- Prepare 3 kg of cement and the corresponding amount of water.  
4- Prepare 8 kg of fine aggregate and 12 kg of coarse aggregate.  
5- Mix the cement prepared with the water to make a cement paste.  
6- From supplies of known weight the aggregates are added in amounts dictated by judgment, with intermittent mixing, until the batch is brought to the desired consistency.  
7- The batch is carefully examined in order to judge which aggregate to add. The correct amount of sand is the minimum which will produce enough mortar to fill the spaces between pieces of coarse aggregate and provide a slight excess for workability. [Undersanding creates harshness whereas oversanding decreases yield, hence a “balanced” mix is desirable.  
8- When the batch is judged to be satisfactory, the remaining supplies of aggregates are weighed and by difference the amounts used in the batch are computed.  
9- Perform a slump test to check the slump.  
10- The mix proportions can be calculated.
Fig. 25. Appearance of (A) undersanded, (B) properly sanded, and (C) oversanded concretes. (Portland Cement Association.)
Test No. 13

“Static Modulus of Elasticity of Concrete in Compression”
( ASTM C 469-87a ) or (BS 1881: Part 121: 1983)

Scope:
This test method covers determination of chord modulus of elasticity (Young’s) of molded concrete cylinders, when under longitudinal compressive stress.

Apparatus:
1-Testing Machine.
2-Compressometer for measuring the average deformation of the gage line (parallel to the axis and centered about midheight of the specimen).

Note:
The effective length of the gage line shall be not less than three times the maximum size of the aggregate in the concrete nor more than two thirds the height of the specimen; the preferred length of the gage line is one half the height of the specimen.

Procedure:
1-It is preferable to use two similar specimen, to determine the compressive strength prior to the test of modulus of elasticity.
2-Place the 2nd specimen, with the strain-measuring equipment attached on the lower platen of the testing machine. Carefully align the axis of the specimen with the center of the machine.
3-Load the specimen at least twice. Do not record any data during the first loading, but observe the performance of the gages and correct any usual behavior prior to the second loading.
4-Apply the load continuously and without shock, at a constant rate (241 ± 34) kPa/s or (3.66-4.86) kN/s.
5-Record, without interruption of loading, the applied load and longitudinal strain.
   The first reading is when the stress equals (0.5 MPa) or the load (8.8 kN) [according to BS], or when the strain is 50 x 10^-6 [according to ASTM].
   The 2nd record is when σ = f_c / 3 [BS], or σ = 0.4 f_c [ASTM].
6-Remove compressometer and continue loading to failure.

Calculations
1- Calculate the modulus of elasticity as follows:

\[ E = \frac{\Delta \sigma}{\Delta \varepsilon} = \frac{(\sigma_2 - \sigma_1)}{(E_2 - E_1)} \]

Where:
\[ E = \text{Secant (chord) modulus of elasticity.} \]
Fig. (26) Fixing the Compressometer for measuring the average deformation of the concrete cylinder.
Concrete Mix Design (Method of Goldbeck and Gray, or b/b₀ method)

The *method of Goldbeck and Gray* has also been called *b/b₀ method* and is sometimes referred to *ACI method*. This method is based on the absolute volumes of the material in a unit volume of concrete. The method takes into account a b/b₀ ratio. The term b equals the volume of coarse aggregate in a unit volume of concrete. The b₀ term equals the solid volume of coarse aggregate in a unit volume of Dry-rodded coarse aggregate. The term b/b₀ equals the dry-rodded volume (Bulk volume) of coarse aggregate in a unit of concrete. The procedure of design of concrete mixtures involves the use of data from tables 1 to 3 which have been prepared by Goldbeck and Gray. These tables are utilizes for typical materials.

The steps in performing a concrete mix design will be listed and then an example will be given.

- b = the solid volume of coarse aggregate in a unit volume concrete.
- b₀ = the solid volume of coarse aggregate in a unit volume of dry-rodded coarse aggregate.
- b/b₀ = the dry-rodded volume of coarse aggregate in a unit volume of concrete.

1. **Concrete Materials**: contains Cement, Water, Coarse Aggregate, and Fine Aggregate.

2. **Concrete Mix Design Procedure**:

   (1) Determine the bulk dry specific gravities of fine and coarse aggregates.

   (2) Determine the dry-rodded unit weight of the coarse aggregate.

   (3) Determine the fineness modulus of the fine aggregates and the absorption of fine and coarse aggregates.

   (4) Compute the solid unit weights of cement, fine aggregate, and coarse aggregate.

   (5) Calculate the b₀ of coarse aggregate as follows:

   \[
   b₀ = \frac{\text{dry - rodded weight/ft}^3}{\text{solid weight/ft}^3}
   \]

   (6) According to the size of coarse aggregate and the fineness modulus of the fine aggregate, find the b/b₀ value from Table 1.

   \[\therefore b = (b/b₀) b₀ = \text{the solid volume of coarse aggregate in a unit volume of concrete}\]
(7) According to the size of coarse aggregate, 28-day compressive strength desired, and slump, find the required water, cement, and air from Table 2 (non-air entrained concrete) or Table 3 (air-entrained concrete).

(8) Determine the solid volumes of cement, water, coarse aggregate, and air and get the total volume of them.

(9) Determine the solid volume of fine aggregate in a cubic yard of concrete as follows:
\[1 \text{ yd}^3 (27 \text{ ft}^3) - \text{sum of item (8)}\]

(10) Convert the solid volumes to lbs/\text{yd}^3 of concrete.

(11) According to the absorption of fine and coarse aggregates, calculate the additional water requirement.

3. **Example:**

**Data**

1. **Coarse Aggregate:**
   a. Size: No. 4 (3/16 in.) to ½ in., angular aggregate
   b. Absorption = 0.4%
   c. Bulk dry specific gravity = 2.7
   d. Dry-rodded unit weight = 101.5 lb/\text{ft}^3

2. **Fine Aggregate:**
   a. Fineness modulus = 2.7
   b. Absorption = 0.8%
   c. Bulk dry specific gravity = 2.5

3. **Concrete:**
   a. 3 in. slump
   b. 3000 psi 28-days compressive strength for non-air-entrained concrete

**Concrete Mix Design**

1. **Coarse Aggregate:**
   Solid unit weight = S.G. × Unit weight of water
   \[= (2.7) (62.4) = 168.48 \text{ (lb/ft}^3)\]

   \[b_o = \frac{\text{dry-rodded weight } / \text{ft}^3}{\text{solid weight } / \text{ft}^3} = \frac{101.5}{168.48} = 0.602\]

   From Table 1, \(b/b_o = 0.56\)
\[ b = \left( \frac{b}{b_0} \right) \cdot b_0 = (0.56)(0.602) = 0.337 \text{ yd}^3 \]

- the solid volume of coarse aggregate in a unit volume of concrete

From Table 2, for No. 4 to ½ in. angular coarse aggregate, 3 in. slump, and 3000 psi 28-days compressive strength, water requirement = 42 gal/yd\(^3\) of concrete

Cement requirement = 5.4 sacks/yd\(^3\) of concrete

Entrained air = 2.5%

2. **Cement:**
   - Specific gravity = 3.14
   - Solid unit weight = (3.14)(62.4) = 195.94 lb/ft\(^3\)
   - 1 sack = 94 lb \(\Rightarrow\) Cement = \((94/195.94) = 0.48\) ft\(^3\) (solid volume)

3. **Water:**
   - 1 ft\(^3\) = 7.5 gallon

4. **Fine Aggregate:**
   - Specific gravity, S.G. = 2.5
   - Solid unit weight = (2.5)(62.4) = 156 lb/ft\(^3\)

5. **Required solid volumes for each material in 1 yd\(^3\) concrete:**
   a. Coarse aggregate: 0.337 yd\(^3\) = \((0.337 \times 27)\) ft\(^3\) = 9.10 ft\(^3\)
   b. Cement: 5.4 (sacks) \(\times\) 0.48 = 2.592 ft\(^3\)
   c. Water: 42 gal = \((42/7.5)\) ft\(^3\) = 5.6 ft\(^3\)
   d. Air: 2.5\% \(\times\) 27 ft\(^3\) = 0.675 ft\(^3\)
   - Total solid volume = 9.10 + 2.592 + 5.6 + 0.675 = 17.967 ft\(^3\)
   e. Fine aggregate: 27 ft\(^3\) – 17.967 ft\(^3\) = 9.033 ft\(^3\)

6. **Convert the solid volume to weight in 1 yd\(^3\) concrete:**
   a. Coarse aggregate: 9.10 \(\times\) 168.48 (solid unit weight) = 1533.17 lb
   b. Cement: 2.592 \(\times\) 195.94 = 507.88 lb
   c. Fine aggregate: 9.033 \(\times\) 156 = 1409.15 lb
   d. Water: 5.6 \(\times\) 62.4 = 349.44 lb
   - Water absorbed by coarse aggregate = 0.4\% \(\times\) 1533.17 = 6.13 lb
   - Water absorbed by fine aggregate = 0.8\% \(\times\) 1409.15 = 11.27 lb
   - Total water: 349.44 + 6.13 + 11.27 = 366.84 lb
   - Total weight in 1 yd\(^3\) concrete = 1533.17 + 507.88 + 1409.15 + 366.84 = 3817.04 lb
   \[\Rightarrow 3817.04/27 = 141.4\] lb/ft\(^3\) of concrete
Notes:

1. Bulk Dry Specific Gravity:
   
   \[ \text{bulk dry specific gravity} = \frac{\text{weight of dry sample}}{\text{ft}^3} \div \frac{\text{weight of water}}{\text{ft}^3} \]

2. Fineness Modulus: The sum of the cumulative weight percentages on a group of 
   
   #4 (0.187 in), #8 (0.0937 in), #16 (0.0469 in), #30 (0.0234 in), #50 (0.0124 in),
   and #100 (0.0059 in) standard sieves in a sieve test of fine aggregate.

3. Slump test: is a measure of consistency of concrete
   
   Procedure: (1) The cone is filled in three layers of approximately equal volume,
   each being rodded 25 times.
   
   (2) Lift the cone and measure the amount slump.

<table>
<thead>
<tr>
<th>Table 4. Recommended Mix Consistencies for Cement</th>
</tr>
</thead>
<tbody>
<tr>
<td><strong>Type of Structure</strong></td>
</tr>
<tr>
<td></td>
</tr>
<tr>
<td>Massive sections, pavement and floors laid on ground</td>
</tr>
<tr>
<td>Heavy slabs, beams, or walls</td>
</tr>
<tr>
<td>Thin walls and columns, ordinary slabs or beams</td>
</tr>
</tbody>
</table>
4. The air-entrained concrete:
The air-entrained concrete is always used during the freezing months. The
entrainment provides the capacity to absorb the expansive forces of ice that form
within the concrete.
The air-entrained concrete can have lower water-cement ratios than non-air-
entrained concrete.


Table 1: DRY-RODDED VOLUME $b/b_0$ OF COARSE AGGREGATE
(ANY TYPE) PER UNIT VOLUME OF CONCRETE*

<table>
<thead>
<tr>
<th>Size of Coarse Aggregate (Square-opening Laboratory Sieves)</th>
<th>Fineness Modulus of Sand</th>
<th>Values* for $b/b_0$</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td></td>
<td>Fineness Modulus of Sand</td>
</tr>
<tr>
<td></td>
<td>Fine Sand</td>
<td>Medium Sand</td>
</tr>
<tr>
<td>2.4 2.5 2.6 2.7 2.8 2.9 3.0 3.1</td>
<td></td>
<td></td>
</tr>
<tr>
<td>No. 4 to ½ in.</td>
<td>0.59</td>
<td>0.58</td>
</tr>
<tr>
<td>No. 4 to ¾ in.</td>
<td>0.66</td>
<td>0.65</td>
</tr>
<tr>
<td>No. 4 to 1 in.</td>
<td>0.71</td>
<td>0.70</td>
</tr>
<tr>
<td>No. 4 to 1½ in.</td>
<td>0.75</td>
<td>0.74</td>
</tr>
<tr>
<td>No. 4 to 2 in.</td>
<td>0.78</td>
<td>0.77</td>
</tr>
<tr>
<td>No. 4 to 2½ in.</td>
<td>0.80</td>
<td>0.79</td>
</tr>
</tbody>
</table>

*From A. T. Goldbeck and J. E. Gray, “A Method of Proportioning Concrete for Strength,
Workability, and Durability,” Bull. 11, National Crushed Stone Association, Nov. 1953.

*bFor concrete that is to be assisted in place by internal vibration under very rigid inspection,
increase tabulated values of $b/b_0$ approximately 10%.
### Table 2: NON-AIR-ENTRAINING STRUCTURAL CONCRETE CEMENT FACTORS REQUIRED FOR 28-DAY COMpressive STRENGTHS LISTED

<table>
<thead>
<tr>
<th>Size of coarse Aggregate Square-opening Laboratory Sieves:</th>
<th>No. 4 to ½ in.</th>
<th>No. 4 to ¾ in.</th>
<th>No. 4 to 1 in.</th>
<th>No. 4 to 1½ in.</th>
<th>No. 4 to 2 in.</th>
<th>No. 4 to 2½ in.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Slump (in.):</td>
<td>3</td>
<td>6</td>
<td>3</td>
<td>6</td>
<td>3</td>
<td>6</td>
</tr>
<tr>
<td>Water* (gal/yd³ of concrete)</td>
<td>42</td>
<td>44</td>
<td>40</td>
<td>42</td>
<td>38</td>
<td>40</td>
</tr>
<tr>
<td>Angular coarse aggregate</td>
<td>36</td>
<td>38</td>
<td>34</td>
<td>36</td>
<td>32</td>
<td>34</td>
</tr>
<tr>
<td>Rounded coarse aggregate</td>
<td>38</td>
<td>40</td>
<td>36</td>
<td>38</td>
<td>34</td>
<td>36</td>
</tr>
</tbody>
</table>

### 28-Day Compressive Strength (psi)

<table>
<thead>
<tr>
<th>Cement (sacks/yd³ of concrete)</th>
<th>4.6</th>
<th>4.8</th>
<th>4.4</th>
<th>4.6</th>
<th>4.2</th>
<th>4.0</th>
<th>4.2</th>
<th>4.0</th>
<th>3.9</th>
<th>4.0</th>
<th>3.8</th>
<th>3.9</th>
</tr>
</thead>
<tbody>
<tr>
<td>2000</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>2500</td>
<td>5.0</td>
<td>5.2</td>
<td>4.8</td>
<td>5.0</td>
<td>4.5</td>
<td>4.8</td>
<td>4.2</td>
<td>4.5</td>
<td>4.1</td>
<td>4.3</td>
<td>4.0</td>
<td>4.2</td>
</tr>
<tr>
<td>3000</td>
<td>5.4</td>
<td>5.7</td>
<td>5.2</td>
<td>5.4</td>
<td>4.9</td>
<td>5.2</td>
<td>4.6</td>
<td>4.9</td>
<td>4.4</td>
<td>4.7</td>
<td>4.3</td>
<td>4.6</td>
</tr>
<tr>
<td>3500</td>
<td>5.9</td>
<td>6.3</td>
<td>5.6</td>
<td>5.9</td>
<td>5.3</td>
<td>5.6</td>
<td>5.0</td>
<td>5.3</td>
<td>4.9</td>
<td>5.2</td>
<td>4.8</td>
<td>5.0</td>
</tr>
<tr>
<td>4000</td>
<td>6.5</td>
<td>6.9</td>
<td>6.2</td>
<td>6.5</td>
<td>5.8</td>
<td>6.2</td>
<td>5.5</td>
<td>5.8</td>
<td>5.4</td>
<td>5.7</td>
<td>5.2</td>
<td>5.5</td>
</tr>
<tr>
<td>4500</td>
<td>7.2</td>
<td>7.5</td>
<td>6.8</td>
<td>7.1</td>
<td>6.4</td>
<td>6.8</td>
<td>6.1</td>
<td>6.4</td>
<td>5.9</td>
<td>6.3</td>
<td>5.7</td>
<td>6.1</td>
</tr>
<tr>
<td>5000</td>
<td>8.1</td>
<td>8.5</td>
<td>7.7</td>
<td>8.1</td>
<td>7.3</td>
<td>7.7</td>
<td>6.9</td>
<td>7.3</td>
<td>6.7</td>
<td>7.1</td>
<td>6.5</td>
<td>6.9</td>
</tr>
</tbody>
</table>

Entrapped air (approx. %) 2.5 2 1.5 1 1 1


*For concrete to be assisted in place by internal vibration, use 3-in. slump and decrease tabulated water contents by approximately 4 gal. No reduction in cement factor is suggested.

*This is water actually effective as mixing water.
Table 3: AIR-ENTRAINING STRUCTURAL CONCRETE CEMENT FACTORS REQUIRED FOR 28-DAY COMPRESSIVE STRENGTHS LISTEDa,b

<table>
<thead>
<tr>
<th>Size of Coarse Aggregate</th>
<th>Laboratory Sieves:</th>
<th>No. 4 to 1/2 in.</th>
<th>No. 4 to 3/4 in.</th>
<th>No. 4 to 1 in.</th>
<th>No. 4 to 1 1/2 in.</th>
<th>No. 4 to 2 in.</th>
<th>No. 4 to 2 1/2 in.</th>
</tr>
</thead>
<tbody>
<tr>
<td>Slump (in.):</td>
<td>3</td>
<td>6</td>
<td>3</td>
<td>6</td>
<td>3</td>
<td>6</td>
<td>3</td>
</tr>
</tbody>
</table>

Water* (gal/yd³ of concrete)

Angular coarse aggregate

|  | 38 | 40 | 36 | 38 | 34 | 36 | 32 | 34 | 31 | 33 | 30 | 32 |

Rounded coarse aggregate

|  | 35 | 37 | 33 | 35 | 31 | 33 | 29 | 31 | 28 | 30 | 27 | 29 |

28-Day Compressive Strength (psi)  Cement (sacks/yd³ of concrete)

| 2000 | 4.4 | 4.7 | 4.2 | 4.4 | 3.9 | 4.2 | 3.7 | 3.9 | 3.6 | 3.8 | 3.5 | 3.7 |
| 2500 | 4.9 | 5.2 | 4.6 | 4.9 | 4.4 | 4.7 | 4.2 | 4.4 | 4.0 | 4.3 | 3.9 | 4.2 |
| 3000 | 5.6 | 5.9 | 5.3 | 5.6 | 5.0 | 5.3 | 4.7 | 5.0 | 4.5 | 4.8 | 4.3 | 4.7 |
| 3500 | 6.3 | 6.7 | 6.0 | 6.3 | 5.6 | 6.0 | 5.3 | 5.6 | 5.1 | 5.4 | 4.9 | 5.3 |
| 4000 | 7.2 | 7.5 | 6.8 | 7.2 | 6.4 | 6.8 | 6.0 | 6.4 | 5.8 | 6.2 | 5.6 | 6.0 |
| 4500 | 8.1 | 8.5 | 7.6 | 8.1 | 7.2 | 7.6 | 6.8 | 7.2 | 6.6 | 7.0 | 6.4 | 6.8 |
| 5000 | 9.2 | 9.7 | 8.7 | 9.2 | 8.2 | 8.7 | 7.7 | 8.2 | 7.4 | 8.0 | 7.2 | 7.7 |

Optimum entrained-air content (%)

| 6.0 | 6.0 | 5.5 | 5.0 | 5.0 | 4.5 |


bThis table should always be used to proportion concrete subject to freezing.

cThis is water actually effective as mixing water.
Steal Testing
1. Introduction:

The most common material in construction besides concrete is steel. Concrete, though it has a high compressive strength, its tensile strength is usually much lower and mounts up to 8 – 12% of its compressive strength. Steel, therefore, is used in concrete structural elements to bare tensile loads and bending moments.

The major components of steel are Iron and carbon which ranges between 0.01 and 1 percent. Sulfur, phosphorus, manganese, silicon and as much as 20 other alloys are present in steel and are added in various quantities to steel during its manufacturing process depending on the desired hardness, toughness and tensile strength of steel.¹

Reinforcing steel bars are usually manufactured in 3 different forms:
- Plain bars
- Deformed bars
- Plain & deformed wires

The deformation in deformed steel bars is intended to increase the bonding between steel and concrete and to prevent slippage of the steel reinforcement bars.
Steel reinforcement bars are produced mainly with four different yield strengths, shown in the table below. The grade of steel indicates its yield strength in Ksi.

<table>
<thead>
<tr>
<th>Type</th>
<th>$\sigma_{\text{yield}}$ (psi)</th>
<th>$\sigma_{\text{yield}}$ (MPa)</th>
<th>Grade</th>
</tr>
</thead>
<tbody>
<tr>
<td>Type 1</td>
<td>40,000</td>
<td>300</td>
<td>40</td>
</tr>
<tr>
<td>Type 2</td>
<td>50,000</td>
<td>350</td>
<td>50</td>
</tr>
<tr>
<td>Type 3</td>
<td>60,000</td>
<td>400</td>
<td>60</td>
</tr>
<tr>
<td>Type 4</td>
<td>75,000</td>
<td>500</td>
<td>75</td>
</tr>
</tbody>
</table>

Table 1: Reinforcement Steel Strength

2. Objectives

The objective of this lab experiments is to incrementally load a steel bar till failure, while recording the value of the load and the change in length of the steel bar at each stage. Then based on the collected data, determine:

- Modulus of Elasticity of Steel, $E_{\text{steel}}$ & Compare it to the theoretical value.
- Yield strength of Steel, $\sigma_{\text{yield}}$
- Ultimate strength of steel, $\sigma_{\text{Ultimate}}$
- Plot Stress Vs Strain Curve for steel

3. Definitions

- Yield Point: The Point at which an increase in strain occurs without an increase in the stress is defined as the yield point. Stress at this point is defined as the steel yield stress.\(^1\)

4. Equipment

- Universal Testing Machine
- Dial Gauge / Extensometer
5. Procedure
1. Load a Steel bar into the machine, with a 6” length of steel between the testing machine clamps.
2. Mount the dial gauge and reset to Zero
3. Apply load with in stages, starting with 250 lb and with increments of 250 lb
4. At each load stage record the applied load and the Change in bar length (read from gauge).
5. Keep incrementing the load till failure.
P.s.: At failure notice the tip & cone failure mode of the steel bar.
6. Equations:

\[
\sigma = \frac{P}{A} \quad \varepsilon = \frac{\delta}{L} \quad E = \frac{\sigma}{\varepsilon} = \frac{\Delta \sigma}{\Delta \varepsilon} \quad A = \frac{\pi d^2}{4} \quad L = 6''
\]

\[
E_{\text{Experimental}} = \frac{\Delta \sigma}{\Delta \varepsilon} \text{(Slope)} \quad \text{or} \quad E_{\text{Experimental}} = E_{\text{ave}}
\]

\[
E_{\text{ave}} = \frac{E_1 + E_2 + E_3 + \ldots + E_m}{m}
\]

\[
E_{\text{Theoretical, Steel}} = 29 \times 10^6 \text{ psi}
\]

\[
\% \text{ Error} = \left| \frac{E_{\text{Experimental}} - E_{\text{Theoretical}}}{E_{\text{Theoretical}}} \right| \times 100\%
\]
7. Typical Stress – Strain Curve

[Diagram showing stress-strain relationship with various points labeled.]

8. Calculation Sheet

<table>
<thead>
<tr>
<th>P (lb)</th>
<th>δ (in)</th>
<th>σ (psi)</th>
<th>ε</th>
<th>E (psi)</th>
</tr>
</thead>
<tbody>
<tr>
<td>250</td>
<td>δ₁</td>
<td>σ₁</td>
<td>ε₁</td>
<td>E₁</td>
</tr>
<tr>
<td>500</td>
<td>δ₂</td>
<td>σ₂</td>
<td>ε₂</td>
<td>E₂</td>
</tr>
<tr>
<td>750</td>
<td>δ₃</td>
<td>σ₃</td>
<td>ε₃</td>
<td>E₃</td>
</tr>
<tr>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
<td>...</td>
</tr>
<tr>
<td>Pₘ</td>
<td>δₘ</td>
<td>(PL) σₘ</td>
<td>εₘ</td>
<td>Eₘ</td>
</tr>
<tr>
<td>...</td>
<td>...</td>
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</tr>
<tr>
<td>Pₙ₋₁</td>
<td>δₙ₋₁</td>
<td>σₙ₋₁</td>
<td>εₙ₋₁</td>
<td>N/A</td>
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<tr>
<td>Pₙ (Pₘₓ)</td>
<td>N/A</td>
<td>σₙ (σₘₓ)</td>
<td>N/A</td>
<td>N/A</td>
</tr>
</tbody>
</table>
9. Discussion

Possible source of error: Slipping of the steel at the testing machine grips

![Diagram of Stress-Strain relationship](image)

Fig. 7. Theoretical Stress-Strain diagram for typical ductile metal.

Lab. Pictures:

![Image of students performing tensile test](image)

Students performing tensile test

![Image of necking of rebar](image)

Necking of the rebar before fracture
1. Introduction

Structural steel elements, besides tensile or compressive loading, might be subject to a third form of loading that is torsion. Turbine shaft, car transmission or a column holding a billboard subject to wind, are all examples of elements subject to torsion. Torsion (torque) results from a force applied at a distance. In other words, torsion results from a Moment (= force x Distance from bar axis) about the axis of a structural element, such as a steel beam or bar.

![Figure 6: Torque on a Steel Bar](image)

What governs the response of steel subject to torsion is its Modulus of Rigidity, $G$ also known as the Shear Modulus. The modulus of rigidity represents a measure of the stiffness of the material in resisting shear loading.
2. Objectives

In this lab experiment two specimens will be used, a brass bar and a steel bar. The dimensions of the bars are as follows:
- \( d_{\text{Steel}} = d_{\text{brass}} = 0.24" \)
- \( L_{\text{steel}} = L_{\text{brass}} = 3.15" \)

Each specimen will be mounted on the Torque Testing Machine, and torque (T) will be applied incrementally. Values of the Torque corresponding to each obtained rotation and the angle of rotation \( \Phi \) (measured using a dial gauge) will be recorded. The collected values for each bar will be used to:
- Determine Modulus of Rigidity, \( G \) and compare it to the theoretical value of \( G \)
- Establish a relationship between \( T & \Phi \), and Plot \( T \) vs. \( \Phi \)
- Establish a relationship between \( \tau & \gamma \), and Plot \( \tau \) & \( \gamma \)

Where:
- \( G \): Modulus of Rigidity, Psi
- \( \Phi \): Rotation, Degrees
- \( T \): Applied torque (Moment), lb-in
- \( \tau \): Shear Stress, Psi
- \( \gamma \): Shear Strain
Figure 8: Sketch of Torsion Test Setup
3. Equipment

- Torsion Testing Machine
- Dial Gauge

![Figure 9: Torsion Testing Machine with bar specimens](image)

4. Procedure

1. Load specimen to the machine
2. Reset Load (Zero Load) gage.
3. Reset Rotation Gage
4. Apply Torque incrementally to obtain desired value of $\Phi$
5. Record values of $T$ and $\Phi$
6. Continue increasing $T$ and recording $T$ and $\Phi$ at each stage.

5. Equations
\[ \tau = \frac{T \times c}{J} \quad \gamma = \frac{c \times \Phi_{\text{radians}}}{L} \quad G = \frac{\tau}{\gamma} \quad J = \frac{\pi \ c^4}{2} \]

\[ G_{\text{Experimental}} = \frac{\Delta \tau}{\Delta \gamma} (\text{Slope}) \quad \text{or} \quad G_{\text{Experimental}} = G_{\text{ave}} \]

\[ G_{\text{ave}} = \frac{G_1 + G_2 + G_3 + \ldots + G_m}{m} \]

\[ \Phi(\text{radians}) = \frac{\Phi_{\text{Deg}}}{180} \pi \]

\[ G_{\text{Theoretical, Steel}} = 10.8 \times 10^6 \text{ psi} \quad G_{\text{Theoretical, Brass}} = 5.6 \times 10^6 \text{ psi} \]

\[ \% \text{ Error} = \left| \frac{G_{\text{Experimental}} - G_{\text{Theoretical}}}{G_{\text{Theoretical}}} \right| \times 100\% \]

6. Typical Graphs

![Graph 1: Torque vs Twist angle](image)
Graph 2: Shearing Stress vs Shearing strain
7. Calculation Sheet

<table>
<thead>
<tr>
<th>$\Phi_{\text{degrees}}$</th>
<th>$T$ (lb-in)</th>
<th>$\Phi_{\text{radians}}$</th>
<th>$\tau$ (psi)</th>
<th>$\gamma$</th>
<th>$G$ (psi)</th>
</tr>
</thead>
<tbody>
<tr>
<td>0.5</td>
<td></td>
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<td></td>
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</tr>
<tr>
<td>1.0</td>
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<td>2.0</td>
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<td>2.5</td>
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<td>3.0</td>
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<tr>
<td>4.0</td>
<td></td>
<td></td>
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<td></td>
<td></td>
</tr>
</tbody>
</table>

8. Discussion
The major Reason of Error: Specimen & Equipment
1. Introduction

Beams subject to lateral loading exhibit a behaviour known as Flexure (Bending). The sagging of a book shelf under the weight of the books is an example of flexure. Under bending the beam experiences 3 types of loading; Compression in the top, tension in the bottom in addition to shear in the direction of the lateral load. The compressive force at the top with the tensile force at the bottom (thus forming a couple) creates what is known as the bending moment.

The degree of flexure of the beam depends on four main factors. Those factors are:
1. The applied load, as load increases the flexure increase
2. Moment of Inertia I of the beam, as the I increases we have less deflection.
3. The length of the beam. Longer spans result in larger deflections
4. The properties of the material making up the beam, mainly E

2. Objectives

Two test specimens will be used. A brass and a cast iron specimen. The specimens have the following dimensions:
- \( h_{\text{Cast Iron}} = h_{\text{brass}} = 6.65 \times 10^{-3} \text{ m} \)
- \( b_{\text{Cast Iron}} = b_{\text{brass}} = 19.94 \times 10^{-3} \text{ m} \)

The specimens will be mounted on the testing machine, and then incremental loads will be applied on the beam. The load will be applied in the form of a pair \( P \) each at a distance “\( a \)” from each support. Dial gauges will be used to measure the deflection at the 2 ends of the specimen and at midspan. The collected data will be used to:

- Determine the Modules of Elasticity \( E_{\text{cast iron}} \) & \( E_{\text{brass}} \) and compare to the theoretical values of \( E \)
- Find a relationship between \( P \) and \( \Delta C \) and plot \( P \) vs. \( \Delta C \)

Figure 10: Sketch of flexure test

3. Equipment
- Flexure Testing Machine
- Dial Gauge
Figure 11: Flexure Testing Machine
4. Procedure
1. Mount specimen on flexure testing machine
2. Reset dial gauges (3 dials)
3. Apply 2 loads of equal value P each at a distance “a” from each support (note the value of “a” to use it in calculations)
4. Incrementally increase load (refers to the indicate loads in the worksheet below)
5. For each load record the readings of the vertical deflections measured by the dial gauges at the specimen ends and midspan.

5. Equations

\[
\delta_s = \frac{\delta_A + \delta_B}{2} \quad \Delta_C = \delta_C - \delta_S \quad I = \frac{1}{12} bh^3
\]

\[
\Delta_C = \frac{P \cdot a \left(3 L^2 - 4 a^2\right)}{24 EI} \quad \text{or} \quad E = \frac{P \cdot a \left(3 L^2 - 4 a^2\right)}{24 \Delta_C I}
\]

\[
L = 1 \, m \quad a = 0.25 \, m
\]

\[
E_{ave} = \frac{E_1 + E_2 + E_3 + \ldots + E_m}{m}
\]

\[
G_{\text{Theoretical,Cast Iron}} = 165 \, GPa \quad G_{\text{Theoretical,Brass}} = 105 \, GPa
\]

\[
\% \, \text{Error} = \left| \frac{E_{\text{Experimental}} - E_{\text{Theoretical}}}{E_{\text{Theoretical}}} \right| \times 100\%
\]
6. Typical Graphs

![Typical Graph](image)

**Figure 12: Typical Load vs Deflection at midspan diagram**

7. Calculation Sheet

<table>
<thead>
<tr>
<th>P (N)</th>
<th>δ_A (m)</th>
<th>δ_B (m)</th>
<th>δ_C (m)</th>
<th>δ_S (m)</th>
<th>Δ_C (m)</th>
<th>E (Pa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>2</td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
<td></td>
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<td>4</td>
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<td>10</td>
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<td></td>
</tr>
<tr>
<td>12</td>
<td></td>
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<td></td>
<td></td>
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<td></td>
</tr>
</tbody>
</table>
8. Discussion

The major reasons of error:

- Specimen
- Equipment

Pictures:

Student performing flexure test in metals

Brass specimen under flexural loads
Wood Testing
**Introduction:**

A buckling load is defined as a critical load or crippling load or Euler’s load on a slender column, which just causes buckling or bending of a compression member. Thus, the nature of compressive force is no more axial in buckling phenomena.

**Objective:**

The main objective is to find theoretical and practical value of buckling load in timber compression members. By performing this lab students will find: the relationship between $\sigma$ and $\varepsilon$ plotting the data obtained and based on the graph identify the proportional Limit (PL), modulus of elasticity $E$, ultimate strength (US), and the relationship between the maximum compressive stress ($F_C$) and the slenderness ratio ($L/d$).

**Procedure:**

Five slender specimens of timber (Southern Pine) are prepared with different square section as follow; sizes (d x d x L): 3"x3"x12", 1.5"x1.5x12", 1"x1"x12", ¾"x¾"x12", and ½"x½"x12". Then they are tested one by one to find out its buckling load. Compressive load is applied slowly on the column specimen until it just starts to buckle and the load is recorded to compare for theoretical value. Theoretically,

$$\text{Buckling load } = P_{cr} = \frac{\pi^2 EI}{(L_e)^2}$$

Where,
- $E$ = elastic modulus of the specimen
- $I$ = $I_{\text{min}}$ = second moment of area (moment of inertia)
- $L_e$ = effective length of column depending on the end condition (in our case, two ends are fixed and hence $L_e$ =‘1.0L’) and $L$ = length of column.
Specimen: Timber slender member with size (bxdx) = 1”x3”x12”,
Equipment: Compression testing machine with load dial gauge.

Result:

### Tables: 3"x3"x12"

<table>
<thead>
<tr>
<th>P (lb)</th>
<th>δ (0.001 in)</th>
<th>σ (psi)</th>
<th>ε</th>
<th>E (psi)</th>
</tr>
</thead>
<tbody>
<tr>
<td>1000</td>
<td>δ₁</td>
<td>σ₁</td>
<td>ε₁</td>
<td>E₁</td>
</tr>
<tr>
<td>2000</td>
<td>δ₂</td>
<td>σ₂</td>
<td>ε₂</td>
<td>E₂</td>
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<tr>
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<td>δ₃</td>
<td>σ₃</td>
<td>ε₃</td>
<td>E₃</td>
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<tr>
<td></td>
<td>……</td>
<td>……</td>
<td>……</td>
<td>……</td>
</tr>
<tr>
<td>Pₘ</td>
<td>δₘ</td>
<td>(PL) σₘ</td>
<td>εₘ</td>
<td>Eₘ</td>
</tr>
<tr>
<td></td>
<td>……</td>
<td>……</td>
<td>……</td>
<td>……</td>
</tr>
<tr>
<td>Pₙ₋₁</td>
<td>δₙ₋₁</td>
<td>σₙ₋₁</td>
<td>εₙ₋₁</td>
<td>N/A</td>
</tr>
<tr>
<td>(Pₘₙ)ₙ</td>
<td>N/A</td>
<td>(σₑₙ max=US) σₙ</td>
<td>N/A</td>
<td>N/A</td>
</tr>
</tbody>
</table>

<table>
<thead>
<tr>
<th>Pₘₙ (lb)</th>
<th>A (in²)</th>
<th>Fₘₙ (Pₘₙ/A) (psi)</th>
<th>L/d</th>
</tr>
</thead>
<tbody>
<tr>
<td>(Pₘₙ)₁</td>
<td>9</td>
<td>(Fₘₙ)₁</td>
<td>4</td>
</tr>
<tr>
<td>(Pₘₙ)₂</td>
<td>A₂</td>
<td>(Fₘₙ)₂</td>
<td>8</td>
</tr>
<tr>
<td>(Pₘₙ)₃</td>
<td>A₃</td>
<td>(Fₘₙ)₃</td>
<td>12</td>
</tr>
<tr>
<td>(Pₘₙ)₄</td>
<td>A₄</td>
<td>(Fₘₙ)₄</td>
<td>16</td>
</tr>
<tr>
<td>(Pₘₙ)₅</td>
<td>A₅</td>
<td>(Fₘₙ)₅</td>
<td>24</td>
</tr>
</tbody>
</table>
Equations:

\[ \sigma = \frac{P}{A}, \quad \varepsilon = \frac{\delta}{L}, \quad E = \frac{\sigma}{\varepsilon} = \frac{\Delta \sigma}{\Delta \varepsilon}, \quad A = d^2, \quad L = 12" \]

\[ E_{\text{experimental}} = \frac{\Delta \sigma}{\Delta \varepsilon} \text{ (slope)} \quad \text{or} \quad E_{\text{experimental}} = E_{\text{ave}} \]

\[ E_{\text{ave}} = \frac{E_1 + E_2 + E_3 + \ldots + E_m}{m}, \quad (E_{\text{theoretical}})_W = 1.3 \times 10^6 \text{ psi} \]

\[ \text{Error (\%)} = \left| \frac{E_{\text{experimental}} - E_{\text{theoretical}}}{E_{\text{theoretical}}} \right| \times 100\%, \quad F_C = \frac{P_{\text{max}}}{A} \]

Figures:
**Discussion:**

It is aimed to be familiar with the buckling load which mainly depends on the modulus of elasticity, moment of inertia of the section, and end condition of the compression member. Possible error may develop due to inferior material quality, eye judgment of buckling and its corresponding load.

The major reason of the error: knots, split, and uneven surface.
Bitumen Testing
SPECIFIC GRAVITY TEST FOR BITUMEN

Theory and Scope:

The density of a bitumen binder is a fundamental property frequently used as an aid in classifying the binders for use in paving jobs. In most applications, the bitumen is weighed, but finally in use with aggregate system, the bitumen content is converted on volume basis. Thus an accurate density value is required for conversion of weight to volume. The specific gravity is greatly influenced by the chemical composition of binder. Increased amount of aromatic type compounds cause an increase in the specific gravity.

The specific gravity is defined by ISI as the ratio of the mass of a given volume of the bituminous material to the mass of an equal volume of water, the temperature of both being specified at 27°C±0.1°C.

The code of practice used to determine the specific gravity is IS: 1202.

Aim: To determine the Specific gravity of given Bituminous material.

Apparatus: There are two methods. 1) Pyknometer Method, 2) Balance Method. Pyknometer Method:

Specific gravity Bottle, Balance and Distilled water.

Procedure:

~ The clean, dried specific gravity bottle is weighed let that be W 1gm.
~ Then it is filled with fresh distilled water and then kept in water bath for at least half an hour at temperature 27°C±0.1°C.
~ The bottle is then removed and cleaned from outside. The specific gravity bottle containing distilled water is now weighed. Let this be W 2gm.

1. ~ Then the specific gravity bottle is emptied and cleaned. The bituminous material is heated to a pouring temperature and the material is poured half the bottle, by taking care to prevent entry of air bubbles. Then it is weighed. Let this be W 3gm.

2. ~ The remaining space in specific gravity bottle is filled with distilled water at 27°C and is weighed. Let this be W 4gm. Then specific gravity of bituminous material is given by formula

\[ \text{Specific Gravity} = \frac{W_1}{W_2} \times \frac{W_3}{W_4} \]
Observation and Calculation:

Result: The specific gravity of given bituminous binder is ____________________ .

Viva Voce:
1. Define specific gravity.
2. What is the use of finding specific gravity?
3. What are the factors affecting specific gravity test?

References:
1. Indian Standard Method for Tar and Bitumen, Determination of Specific Gravity of Bitumen, IS: 1202, Indian Standards Institution.
PENETRATION TEST

Theory and Scope:

The consistencies of bituminous materials vary depending upon several factors such as constituents, temperature, etc. As temperature ranges between 25° and 50°C most of the paving bitumen grades remain in semi solid or in plastic states and their viscosity is so high that they do not flow as liquid.

Determination of absolute viscosity of bituminous material is not so simple. Therefore the consistency of these materials is determined by indirect methods. The consistency of bitumen is determined by penetration test which is a very simple test. Various types and grades of bituminous materials are available depending on their origin and refining process. The penetration test determines the consistency of these materials for the purpose of grading them, by measuring the depth (in units of one tenth of a millimeter or one hundredth of a centimeter) to which a standard needle will penetrate vertically under specified conditions of standard load, duration and temperature. Thus the basic principle of the penetration test is the measurement of the penetration (in units of one tenth of a mm) of a standard needle in a bitumen sample maintained at 25°C during five seconds, the total weight of the needle assembly being 100gm. The softer the bitumen, the greater will be the penetration. The test is conducted as per IS-1203 for paving bitumen.

Aim: To determine the grade of a given binder.

Apparatus: It consists of items like container, needle, water bath, penetrometer, stop watch etc.

1. Container is 55mm in diameter and 35mm to 57mm height. The needle is provided with a shank approximately 3.0mm in diameter into which it is immovably fixed.

2.
**Procedure:**

~ The bitumen is softened to a paving consistency between 75° and 100°C above the approximate temperature at which bitumen softens.

~ The sample material is thoroughly stirred to make it homogeneous and free from air bubbles and water.

~ The sample containers are cooled in atmosphere of temperature not lower than 13°C for one hour. Then they are placed in temperature controlled water bath at a temperature of 25°C for a period of one hour.

~ The weight of needle, shaft and additional weight are checked. The total weight of this assembly should be 100gm.

~ Using the adjusting screw, the needle assembly is lowered and the tip of the needle is made to just touch the top surface of the sample.

~ The needle assembly is clamped in this position. The contact of the tip of the needle is checked using the mirror placed on the rear of the needle.

~ The initial reading of the penetrometer dial is either adjusted to zero or the initial reading is noted.

~ Then the needle is released by pressing a button and a stop watch is started. The needle is released exactly for a period of 5.0secs.

~ At least 3 measurements are made on this sample by testing at distance of not less than 100mm apart.

~ The difference between the initial and final penetration readings are taken as the penetration value.
Penetrometer

**Observation and Calculation:**

<table>
<thead>
<tr>
<th>Mean Value</th>
<th>Trails</th>
<th>Readings</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>3</td>
<td>2</td>
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</tr>
</tbody>
</table>
Result:
The average penetration value of a given bitumen sample is ________________ and the grade of bitumen is ________________.

Viva Voce:
1. What are the applications of penetration test?
2. What do you understand by the term 30/40 bitumen?
3. What are the precautions to be taken while conducting a penetration test?

References:
DUCTILITY TEST

Theory and Scope:
A certain minimum ductility is necessary for a bitumen binder. This is because of the temperature changes in bituminous mixes and the repeated deformations that occur in flexible pavements due to the traffic loads. It is of significant importance that the binders form ductile thin films around the aggregates. The binder material which does not possess sufficient ductility would crack and thus provide previous pavement surface. This in turn results in damaging effect to the pavement structure. The ductility is expressed as the distance in centimeters to which a standard briquette of bitumen can be stretched before the thread breaks. The test is standardized by the IS: 1208. The test is conducted at 27°C±0.5°C and a rate of pull of 50±2.5 mm per minute.

Aim: To conduct ductility test on given bitumen sample.

Apparatus: Briquette mould, (length - 75mm, distance between clips - 30mm, width at mouth of clips - 20mm, cross section at minimum width - 10mm x 10mm), Ductility machine with water bath and a pulling device at a precalibrated rate, a putty knife, thermometer.

Procedure:
~ The bitumen sample is method to a pouring temperature (75°C to 100°C) and poured into the mould assembly and placed on a brass plate, where a solution of glycerin or soap solution is applied at all surfaces of briquette mould exposed to bitumen.
~ After the sample is poured to the mould, thirty to forty minutes the entire assembly is placed in a water bath at 27°C.
~ Then the sample is removed from the water bath maintained at 27°C and excess bitumen material is cutoffby leveling the surface using hot knife.
~ After trimming the specimen, the mould assembly containing sample is replaced in water bath maintained at 27°C for 85 to 95 minutes. Then the sides of mould are removed and
the clips are carefully booked on the machine without causing any initial strain. Two or more specimens may be prepared in the moulds and clipped to the machine so as to conduct these tests simultaneously.

~ The pointer is set to read zero. The machine is started and the two clips are thus pulled apart horizontally.

~ While the test is in operation, it is checked whether the sample is immersed in water at a depth of at least 10 mm. The distance at which the bitumen thread of each specimen breaks is recorded (in cm) to report as ductility value.

![Ductility Test Concept](image)

Sample Prepared in Briquette Mould and Ductility Apparatus
Observation and Calculation:

<table>
<thead>
<tr>
<th>Mean Value</th>
<th>Trails</th>
<th>Test Property</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>3</td>
<td>2</td>
</tr>
</tbody>
</table>

Result: The ductility value of the given bitumen sample is ________________ cm.

Viva Voce:
1. List the factors that affect the result of a ductility test.
2. What do you understand by the term repeatability and reproducibility? 3. Explain the significance of ductility test.

References:
SOFTENING POINT OF BITUMEN

Theory and Scope:

Bitumen does not suddenly change from solid to liquid state, but as the temperature increase, it gradually becomes soften until it flows readily. The softening point is the temperature at which the substance attains particular degree of softening under specified condition of test. For bitumen it is usually determined by Ring and Ball apparatus. The test is conducted as per IS: 1205.

Aim: To determine the softening point of given paving bitumen as per IS: 1205.

Apparatus: Ring and Ball apparatus, Water bath with stirrer, Thermometer, Glycerin, etc. Steel balls each of 9.5mm and weight of 2.5±0.08gm.

Procedure:

~ Sample material is heated to a temperature between 75° and 100°C above the approximate softening point until it is completely fluid and is poured in heated rings placed on the metal plate.
~ To avoid sticking of the bitumen to metal plate, coating is done to this with a solution of glycerin and dextrin.
~ After cooling the rings in air for 30 minutes, the excess bitumen is trimmed and rings are placed in the support.
~ At this time the temperature of distilled water is kept at 5°C. This temperature is maintained for 15 minutes after which the balls are placed in position.
~ Then the temperature of water is raised at uniform rate of 5°C per minute with a controlled heating unit, until the bitumen softens and touches the bottom plate by sinking of balls. At least two observations are made. For material whose softening point is above 80°C, glycerin is used for heating medium and the starting temperature is 35°C instead of 5°C.
~ The temperature at the instant when each of the ball and sample touches the bottom plate of support is recorded as softening point value.

Softening Test Concept

Softening Point Apparatus and Ring and Ball Guides
Observation and Calculation:

<table>
<thead>
<tr>
<th>Mean Value</th>
<th>Trails</th>
<th>Test Property</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>3</td>
<td></td>
</tr>
<tr>
<td></td>
<td>2</td>
<td></td>
</tr>
<tr>
<td></td>
<td>1</td>
<td>Temperature (°C) at which I ball touches the bottom plate</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Temperature (°C) at which II ball touches the bottom plate</td>
</tr>
<tr>
<td></td>
<td></td>
<td>Final Softening Point Temperature</td>
</tr>
</tbody>
</table>

Result: The softening point value of given bitumen sample is ____________________________  oC and grade of bitumen is _________________ .

Viva Voce:

1. What are the factors which affect the ring and ball test results? 2. What is softening point?

   If material A has softening point of 56 and B has 42 which binder is good and why?

References:

1. Indian Standard Method for Tar and Bitumen, Determination of Softening Point of Bitumen, IS: 1205, Indian Standards Institution.
FLASH AND FIRE POINT TEST

Theory and Scope:

Flash and Fire point test is a safety test conducted on a bituminous material so that it gives an indication of the critical temperature at and above where precautions should be taken to eliminate fire hazards during its applications. Bituminous materials leave out volatiles at high temperature depending upon their grade. These volatile vapors catch fire causing a flash. This condition is very hazardous and it is therefore essential to qualify this temperature for each bitumen grade, so that the paving engineers may restrict the mixing or application temperature well within the limits. Flash and Fire point test is conducted as per IS: 1209.

As per IS: 1209 the definitions of flash and fire point are:

Flash Point: "The flash point of a material is the lowest temperature at which the vapour of substance momentarily takes fire in the form of a flash under specified conditions of test".

Fire Point: "The fire point is the lowest temperature at which the material gets ignited and burns under specified condition of test".

Aim: To determine the flash and fire point of a given bituminous material.

Apparatus: Pensky-Martens closed cup tester, thermometer, heating source, flame exposure.

Procedure:

~ All parts of the cup are cleaned and dried thoroughly before the test is started.
~ The material is filled in the cup upto a mark. The lid is placed to close the cup in a closed system.
    All accessories including thermometer of the specified range are suitably fixed.
~ The bitumen sample is then heated. The test flame is lit and adjusted in such a way that the size of a bed is of 4mm diameter. The heating of sample is done at a rate of 5° to 6°C per minute. During heating the sample the stirring is done at a rate of approximately 60 revolutions per minute.
~ The test flame is applied at intervals depending upon the expected flash and fire points and corresponding temperatures at which the material shows the sign of flash and fire are noted.

Flash and Fire Point Test Concept

Flash and Fire Point Test in Progress
Observation and Calculation:

<table>
<thead>
<tr>
<th>Mean Value</th>
<th>Trails</th>
<th>Test</th>
</tr>
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<tr>
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<td>3</td>
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</table>

Flash Point
Fire point

Result: The temperature at which the flame application that causes a bright flash ______ oC and temperature at which the sample catches fire ______________________ oC.

Viva Voce:
1. Define flash and fire points.
2. What is the significance of flash and fire point test?
3. What are the parameter that affects the result of flash and fire point tests?

References:
VISCOSITY TEST

Theory and Scope:
Viscosity is defined as the increase of fluidity. The degree of fluidity at the application temperature greatly influences the ability of bituminous material to spread, penetrate into void and also coat the aggregates and hence affects the strength characteristics of the resulting paving mixes. There is an optimum value of fluidity or viscosity for mixing and compacting for each aggregate gradation of the mix and bitumen grade. At high fluidity or low viscosity, the bitumen binder simply "lubricates" the aggregate particles instead of providing a uniform film thickness for binding action. Similarly, low fluidity or high viscosity does not enable the bitumen to coat the entire surface of aggregates. It will increase the compactive force or effort. The test is conducted as per IS: 1206.

Aim: To determine the property of a given bituminous material as per IS: 1206.

Apparatus: A orifice viscometer (one of 4.0mm diameter used to test cut back grades 0 and 1 and 10mm orifice to test all other grades), water bath, stirrer and thermometer.

Procedure:
~ The tar cup is properly leveled and water in the bath is heated to the temperature specified for the test and is maintained throughout the test.
~ The sample material is heated at the temperature 20 above the specified test temperature and the material is allowed to cool. During cooling the material continuously, stirred.
~ When material reaches slightly above test temperature, the same is poured in the tar cup, until the leveling peg on the value rod is just immersed.
~ A graduate receiver (cylinder) and a 20ml of mineral oil or one percent by weight solution of soft soap is poured.
~ When the sample material reaches the specified test temperature within ±0.1°C and then valve is opened.
The stop watch is started with the valve opening and time is noted for collecting a 50ml of test sample to flow through the orifice and collected in the receiver kept below the orifice viscometer.

Schematic Representation of Experiment

Standard Tar Viscometer
Observation and Calculation:

<table>
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</table>

**Result:** The time in seconds for 50ml of the test sample to flow through the orifice.

**Viva Voce:**
1. Explain the term viscosity.
2. What are the uses of viscosity test?
3. What are the precautions to be taken during viscosity test using orifice viscometer?

**References:**
**Bituminous Mix Design by Marshall Method**

**Theory and Scope:**

Bituminous mixes are used in the surface course of road and airfield pavements. The desirable bituminous mix properties include stability, density, durability, flexibility, resistance to skidding and workability during construction. Stability is defined as resistance of the paving mix to deformation under load and is thus a stress level which causes strain depending upon anticipated field conditions. Stability is function of friction and cohesion. Durability is defined as the resistance of the mix against weathering which causes hardening and this depends upon loss of volatiles and oxidation.

In this method the resistance to plastic deformation of cylindrical specimen of bituminous mixture is measured when the same is loaded at the periphery at 5 cm per minute. This test procedure is used in designing and evaluating bituminous paving mixes. ASTM vide designation D 1559-62 T has standardized the test procedure.

**Aim:** To determine optimum binder content of given bituminous mix by Marshall method of Mix Design.

**Apparatus:** Mould Assembly, Sample Extractor, Compaction Pedestal and Hammer, Breaking Head, Loading Machine, flow meter, thermometers, water bath and oven.

**Procedure:**

~ The coarse aggregates, fine aggregates and mineral filler material should be proportioned and mixed in such a way that final mix after blending has the gradation within the specified range.

~ Approximately 1200 grms of aggregates and filler are taken and heated to a temperature of 175° to 190° C.

~ The compaction mould assembly and rammer are cleaned and kept pre-heated to a temperature of 100°C to 145°C. The bitumen is heated to temperature of 121 ° to 138° C
and the required quantity of first trial percentage of bitumen is added to the heated aggregate and thoroughly mixed using a mechanical mixer or by hand mixing with trowel.

- Then the mix is heated and a temperature of 150° to 160°C is maintained and then the mix is transferred into the pre-heated mould and compacted by giving seventy five blows on each side.
- The specific gravity values of different aggregates, filler and bitumen used are determined first. The theoretical specific gravity of the mix is determined.
- Soon after the compacted bituminous mix specimens have cooled to room temperature, the weight, average thickness and diameter of the specimen are noted. The specimens are weighed in air and then in water.
- The bulk density value of the specimen if calculated from weight and volume.
- Then the specimen to be tested are kept immersed under water in a thermostatically controlled water bath maintained at 60° ± 1 °C for 30 to 40 minutes.
- The specimens are taken out one by one, placed in the Marshall test head and the Marshall stability value and flow value are noted.
- The corrected Marshall Stability value of each specimen is determined by applying the appropriate correction factor, if the average height of the specimen is not exactly 63.5 mm.

- Five graphs are plotted with values of bitumen content against the values of density, Marshall Stability, Voids in total mix, Flow value, Voids filled by Bitumen.
- Let the bitumen contents corresponding to maximum density be B₁, corresponding to maximum stability be B₂ and that corresponding to the specified voids content (at 4.0%) be B₃. Then the optimum bitumen content for mix design is given by: Bo= (B₁+ B₂+ B₃) / 3
1. Materials Selection

2. Design Aggregate Structure

3. Preparation of Specimen

4. Design Binder Content

Steps Showing the Procedure of Marshall Mix Design
Pictorial Representation of Marshall Mix Design
**Observations and Calculations:**

**Result:** The optimum binder content of the given mix is ____________________

**Viva Voce:**

1. What is the significance of flow value in Marshall Test?
2. What is filler?
3. What are the essential properties of bituminous mixes?

**Reference:**

2. Ministry of Road Highway Transport, fourth revisions, by Indian Road Congress.